

1670 Mercer St. Windsor | Ontario N8X 3P7 Tel 519.254.3430 ada-architect.ca

May 08, 2024

## **Open House Report**

Re: Stage 2 Planning Consultation Application (0 Howard Avenue, Roll No. 080-060-01100) Applicant – RAFCO Property Trust Ltd.

To Whom it May Concern:

Architectural Design Associates Inc. Architect (ADA) was retained to organize a public open house in preparation for the submission of a Stage 2 Planning Consultation Application (PC2), on behalf of the Applicant, RAFCO Property Trust Ltd. (Zeyad Rafih).

The open house was held at 4350 Howard Avenue (Antonino's Original Pizza), approximately 150m from the subject site. The open house was held between 4:30PM and 6:30PM on Monday, April 8<sup>th</sup>, 2024. A copy of the notice provided to nearby property owners can be found in **Appendix A**. The sign-in sheet provided for nearby property owners can be found in **Appendix B**. Also in attendance were the following:

- Zeyad Rafih Property Owner and Applicant
- Jerry Kavanaugh ADA Representative
- Olivia Byrne ADA Representative
- Adam Szymczak City of Windsor Representative

During the open house, conceptual architectural packages and enlarged display boards were available for residents to review. A copy of the conceptual packages can be found in **Appendix C**. Additionally, copies of the noise study, sanitary sewer study, and storm sewer study prepared for this application were available for residents to review. Copies of these reports can be found in **Appendices D through F**.

#### **Summary of Comments**

Neighbouring residents were mostly concerned with three items:

- a) Parking Provided
  - <u>Concern</u>: Residents of Howard Place were concerned that the parking provided for the development would be inadequate for the number of residents, and that overflow parking would occur along Howard Place

• <u>Response</u>: The parking provided was based on the City of Windsor By-law 8600 requirement for a "Multiple Dwelling containing a minimum of 5 Dwelling units". The By-law requires 1.25 spaces per dwelling unit:

1.25 spaces / unit x 18 units = 22.5 spaces = **22 spaces** (per 24.20.7.3)

#### b) Refuse Enclosure

- <u>Concern</u>: Residents of Howard Place were concerned with the location and visibility of the refuse enclosure
- Response: The refuse enclosure initially proposed is consistent with the City of Windsor standards. Additionally, there is a mature tree line along Howard Place that screens a large part of the development – all parties involved are committed to preserving as many of these trees as possible. The option of individual roll-out containers was also discussed, and an alternative site plan has been developed for curbside pickup in lieu of overhead collection in the parking lot (see Appendix G).

#### c) Environmental Remediation

Olivia Byrne

- <u>Concern</u>: Long-established residents expressed concern about the environmental remediation of the site and its previous use having been a gas station
- Response: As no environmental assessment of the property was required for the PC2 Application, no copy of the existing report was provided at the open house. A subsurface investigation was conducted by Central Projects Group Inc. in 1992 for the purposes of divestment and potential sale of the property; a copy of this report can be found in Appendix H. It was discussed with residents that should any future environmental studies or remediation need to be done for the development of the property, they would be completed as required and by qualified professionals.

to cor	Should you have any questions on the antact us.	ibove or the enclosed, please do not hesitate
Writte	n by:	Reviewed By:

Jerry Kavanaugh



#### March 21st, 2024

#### **RE: PUBLIC CONSULTATION MEETING**

#### PROPOSED DEVELOPMENT - 0 HOWARD AVENUE

Dear Neighboring Resident: I am the owner of the property located at 0 Howard Avenue, the property bounded by Howard Avenue, Howard Place, and Tuson Way (more specifically shown by the attached map). I am looking to develop this property as a small-scale multi-residential development, consisting of three 6 plex buildings. Since this property is currently zoned for commercial development, I am in the process of completing a Zoning Bylaw Amendment (ZBA) application. Prior to applying to the City of Windsor Planning Department, I would like to take the opportunity to share the proposal in more detail with you.

The purpose of this meeting is to provide a discussion for the applicant and surrounding property owners/residents to review the proposal and to identify any issues so that they may be considered before a ZBA application is submitted to the City. This meeting gives you the opportunity to share with me any concerns or feedback regarding the planned development. My architectural team and I will gather your comments for consideration and incorporate them into the development where possible, feasible and appropriate.

You are invited to attend meeting on:

Monday, April 8th between 4:30PM and 6:00PM, at

Antonino's Original Pizza (4350 Howard Avenue)

Please note this meeting will be an informational meeting based on preliminary development plans, which may be altered prior to final submittal of the application to the City. However, these plans were developed to give the public a realistic understanding of the look and scale of this development. I look forward to discussing this proposal with you in detail. Complimentary refreshments will also be provided.

Sincerely,

Zeyad Rafih

Rafco Property Trust Ltd.

# ArcGIS Web Map









1670 Mercer St. Windsor | Ontario N8X 3P7 Tel 519.254.3430

ada-architect.ca

**Public Consultation Sign-in Sheet** 

Date: Monday, APRIL 8, 2024 (4:30PM-6PM)
Address Name(s)

Sign-In

Address	name(s)		sign-in
0 DOUGALL AVE	WINDSOR CITY		
0 HOWARD AVE	RAFCO PROPERTY TRUST LIMITED		
545 NORTH TALBOT RD	DESJARDINS, PATRICIA KELLIE	DESJARDINS, MICHAEL	
4292 HOWARD PL	HORMIZ, MAGED	YOUNAN, NUHA	
365 NEAL BLVD	PUTRUS, ALAA TONY		
4235 DOUGALL AVE	BORDIGNON, DAVID	BORDIGNON, JACQUELINE	
4245 DOUGALL AVE	ZILA, SAMUEL	ZILA, ELIZABETH	
4265 DOUGALL AVE	DAWSON, DWAYNE ALLAN	DAWSON, SANDRA EVE	
4275 DOUGALL AVE	PATEL, RADHA		
4230 HOWARD PL	MORROW, DANIEL GEORGE		2 Smille
4240 HOWARD PL	MILLAR, CATHERINE MACAULEY	·	3 Amilla
4252 HOWARD PL	MILLAR, CATHERINE		5
4262 HOWARD PL	SHAW, RAYMOND LLOYD		
4270 HOWARD PL	HABIB, MARIA		
4272 HOWARD PL	ALEJANDRIA, ALEXANDER GIL	ALEJANDRIA, SHARRON LEE	
4276 HOWARD PŁ	POTRUS, KLARA		
4284 HOWARD PL	DIFAZIO, ASSUNTA		
4286 HOWARD PL	FARDELLA, SIMONE	FARDELLA, CONCETTA	10
4298 HOWARD PL	GIROUX, JEAN	VERONNEAU, CORINNE	15
4300 HOWARD AVE	1486062 ONTARIO INC		4
4248 KENNEDY DR E	SEFEROVIC, PETAR		il in
4258 KENNEDY DR E	SPANOS, JIM	SPANOS, MARY	
4266 KENNEDY DR E	BAKO, LESLIE LASZLO		
4272 KENNEDY DR E	LENISA, ROSE MARIE ANN		
4278 KENNEDY DR E	RETTIG, STEVEN	RETTIG, CHRISTINA	
4284 KENNEDY DR E	BRKLACIC, SARAH CATHERINE	LARABEE, JUSTIN MATTHEW	
4290 KENNEDY DR E	REALE, DONATO		
320 NEAL BLVD	MALLET, GILBERT JOSEPH	MALLET, NORA MARIE	
330 NEAL BLVD	TRIM, DEBRA SUE	Ted Trim	19 1005
340 NEAL BLVD	BOXE, VERNON JOSEPH	BOXE, CYNTHIA ELĘENE	(4) 1/3
360 NEAL BLVD	MOHSEN, MANSOUR		- 12
4296 KENNEDY DR E	ZHENG, CHAO	Li, Qi	/
530 NORTH TALBOT RD	RIDDICK, SAMUEL WALTER	RIDDICK, JOSEPHINE BERTHA	0.0
535 NORTH TALBOT RD	CIARAVINO, GIUSEPPE		9C
540 NORTH TALBOT RD	BIASI, FRANCO LOUIE	BIASI, ANGELA	A.

4210 Howard. John Revoul.



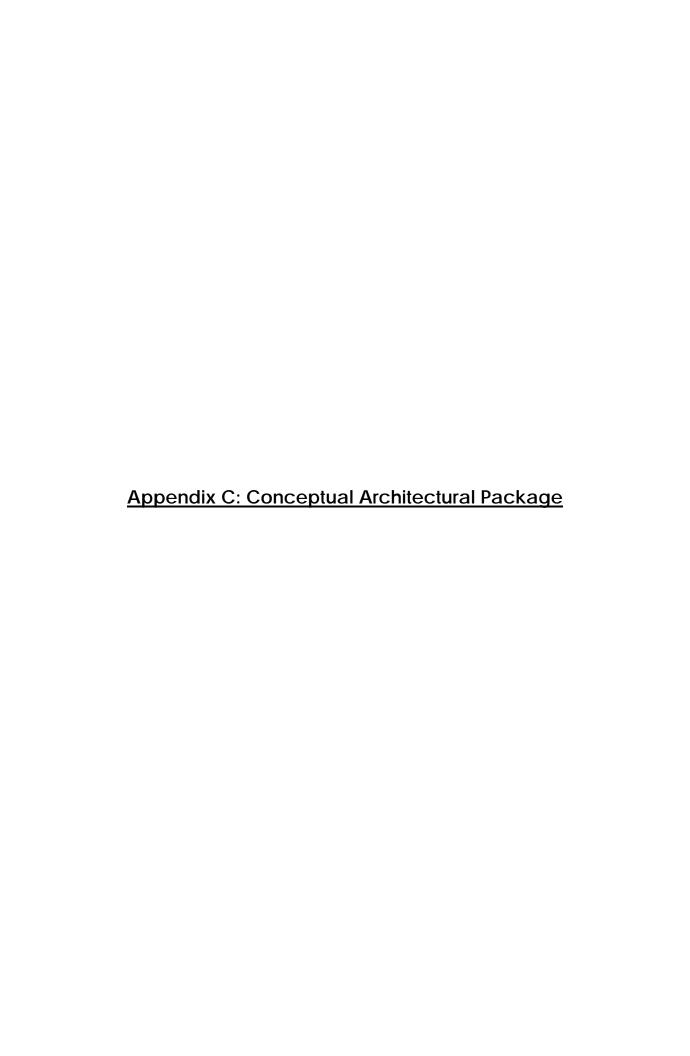
# **Public Consultation Sign-in Sheet**

Date:

Address Name(s)

Sign-In

Addiess	1141110(0)		0.9
333 BARTLET DR	CHAMI, SOURAYA		
355 BARTLET DR	OLLETT, CHRISTOPHER	RANGER OLLETT, CAROL	
540 NTalbet	Bet Carl Gualtica, 1339456 ONTARIO Klava Dotras		
4240 HOWARD	Carl GHALTIBEI	(RENTER)	and the
4350 HOUNAR	1339456 ONTARIO	(17)-	AC
4276 HOW	Klava Dotrus		000
	THE PLANT FOR THE PARTY OF THE		
			0
		19-18/14/ES-04-FQ	



# O HOWARD AVENUE, WINDSOR, ON PROPOSED MULTI-RESIDENTIAL DEVELOPMENT

RENDER PACKAGE







1670 Mercer St. Windsor | Ontario N8X 3P7

Tel 519.254.3430

ada-architect.ca



0 Howard Avenue, Windsor, ON







1670 Mercer St. Windsor | Ontario N8X 3P7

Tel 519.254.3430 ada-architect.ca



0 Howard Avenue, Windsor, ON







1670 Mercer St. Windsor | Ontario N8X 3P7

Tel 519.254.3430

ada-architect.ca



0 Howard Avenue, Windsor, ON







1670 Mercer St. Windsor | Ontario N8X 3P7

Tel 519.254.3430 ada-architect.ca



0 Howard Avenue, Windsor, ON

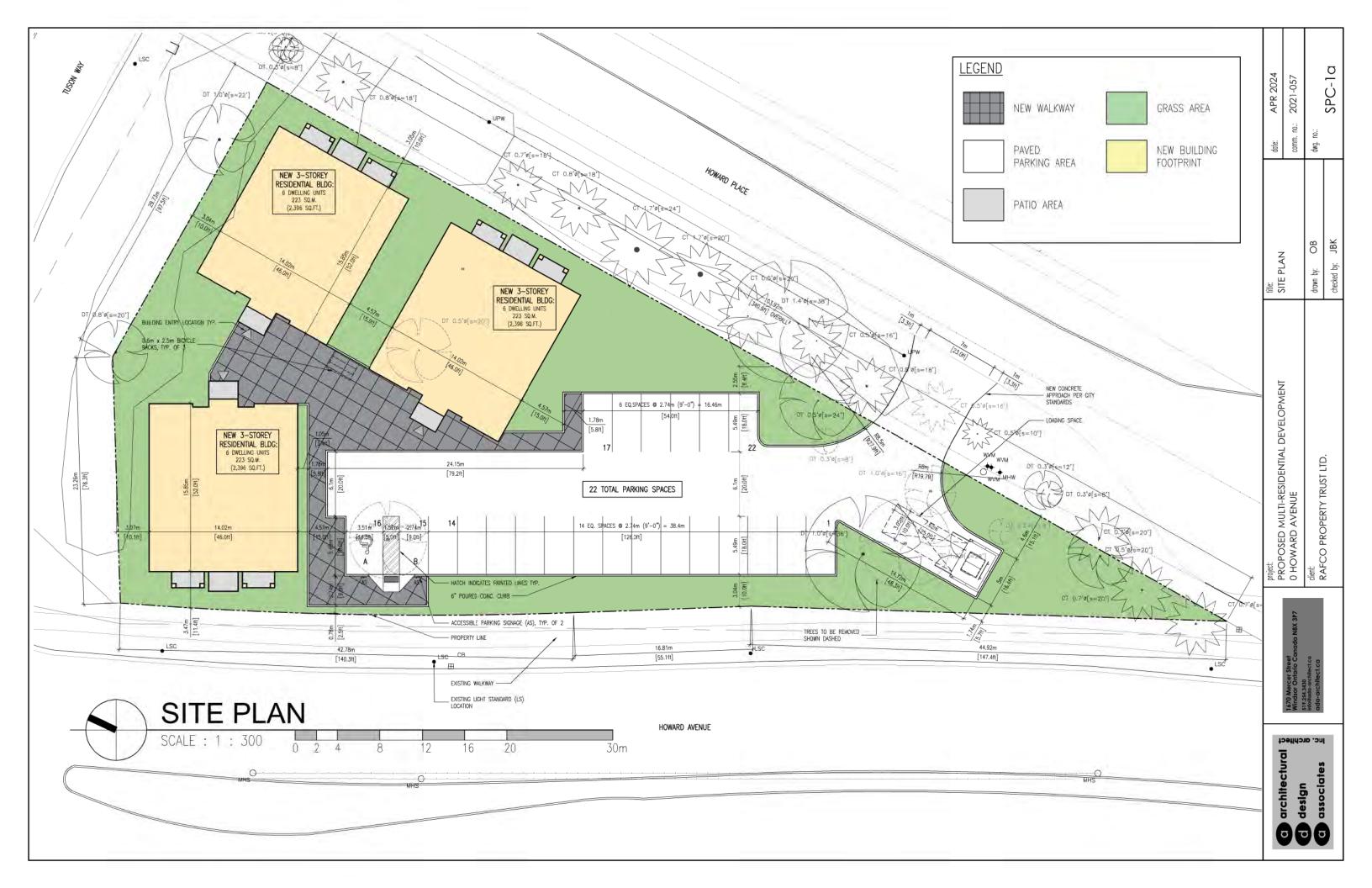


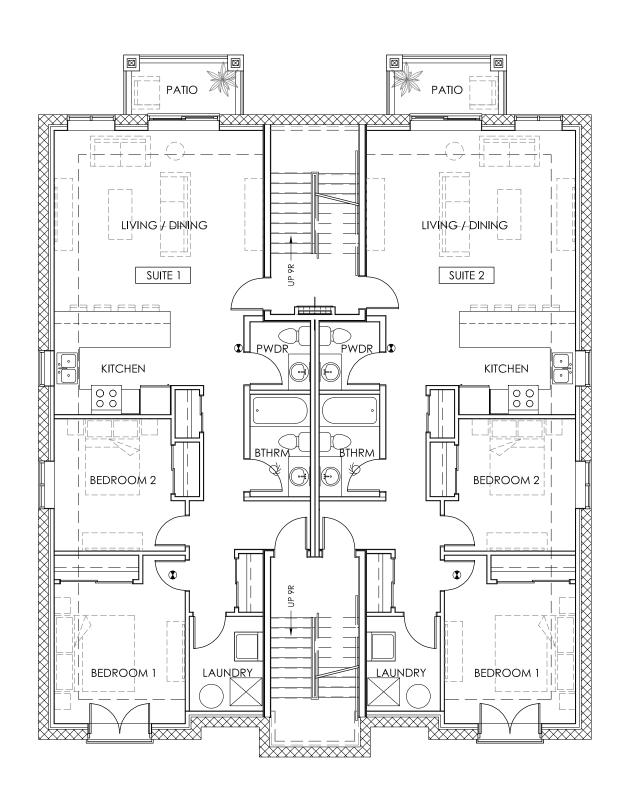




1670 Mercer St. Windsor | Ontario N8X 3P7

Tel 519.254.3430 ada-architect.ca



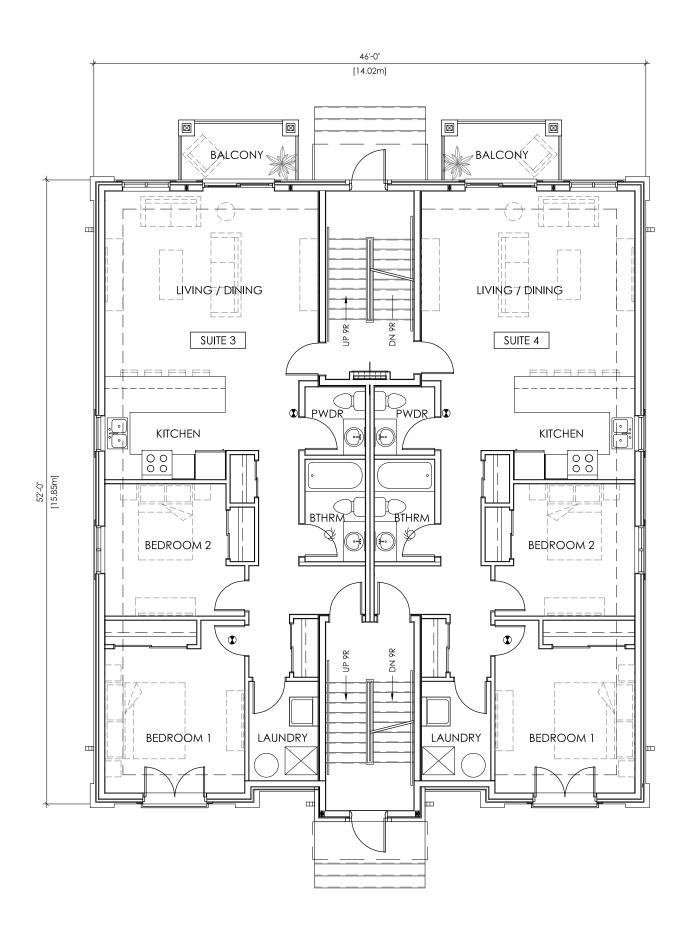




architectural	fect
design	arch.
associates associates	Ē

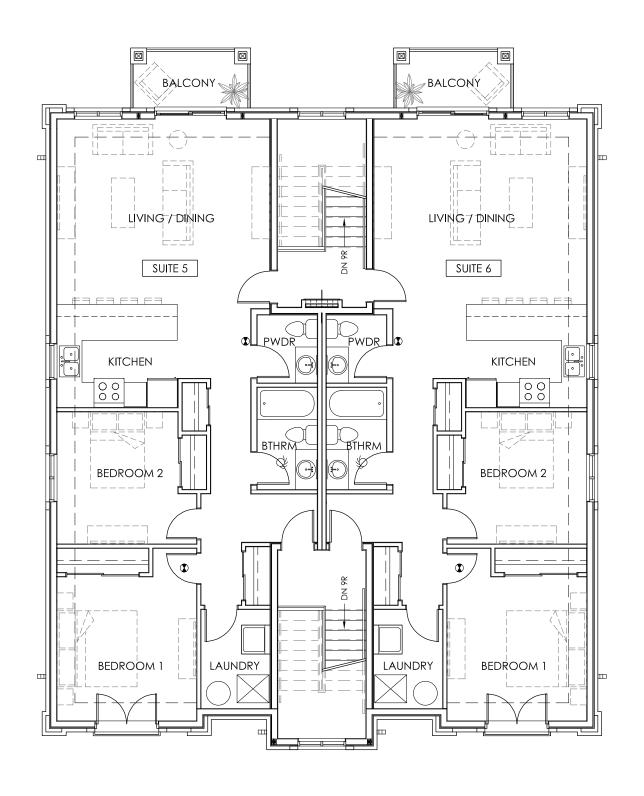
1670 Mercer Street Windsor Ontario Canada N8X 3P7 519:254:3430 into@ada-architect.ca ada-architect.ca

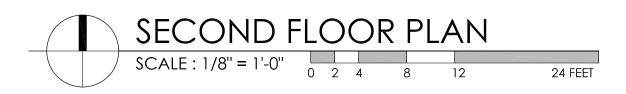
project: PROPOSED MULTI-RESIDENTIAL DEVELOPMENT	title: LOWER FLOOR PLAN	date:	APR 2024
0 HOWARD AVENUE	LO WERT LO GIVE EA WY	comm. no.:	2021-057
client: RAFCO PROPERTY TRUST LTD.	drawn by: OB	dwg. no.:	
KAI GOT KOI EKIT IKOSI EID.	checked by: JBK		SK-1





architectural 7		project: PROPOSED MULTI-RESIDENTIAL DEVELOPMENT	title: FIRST FLOOR PLAN	date: APR 2024	
design	1670 Mercer Street Windsor Ontario Canada N8X 3P7 519.254.3430	0 HOWARD AVENUE	THOTTEGORY EXT	comm. no.: 2021-057	
associates <u>ë</u>	info@ada-architect.ca ada-architect.ca	client: RAFCO PROPERTY TRUST LTD.	drawn by: OB	dwg. no.:	1
		KAI GO I KOI EKTI IKOSI EID.	checked by: JBK	SK-2	

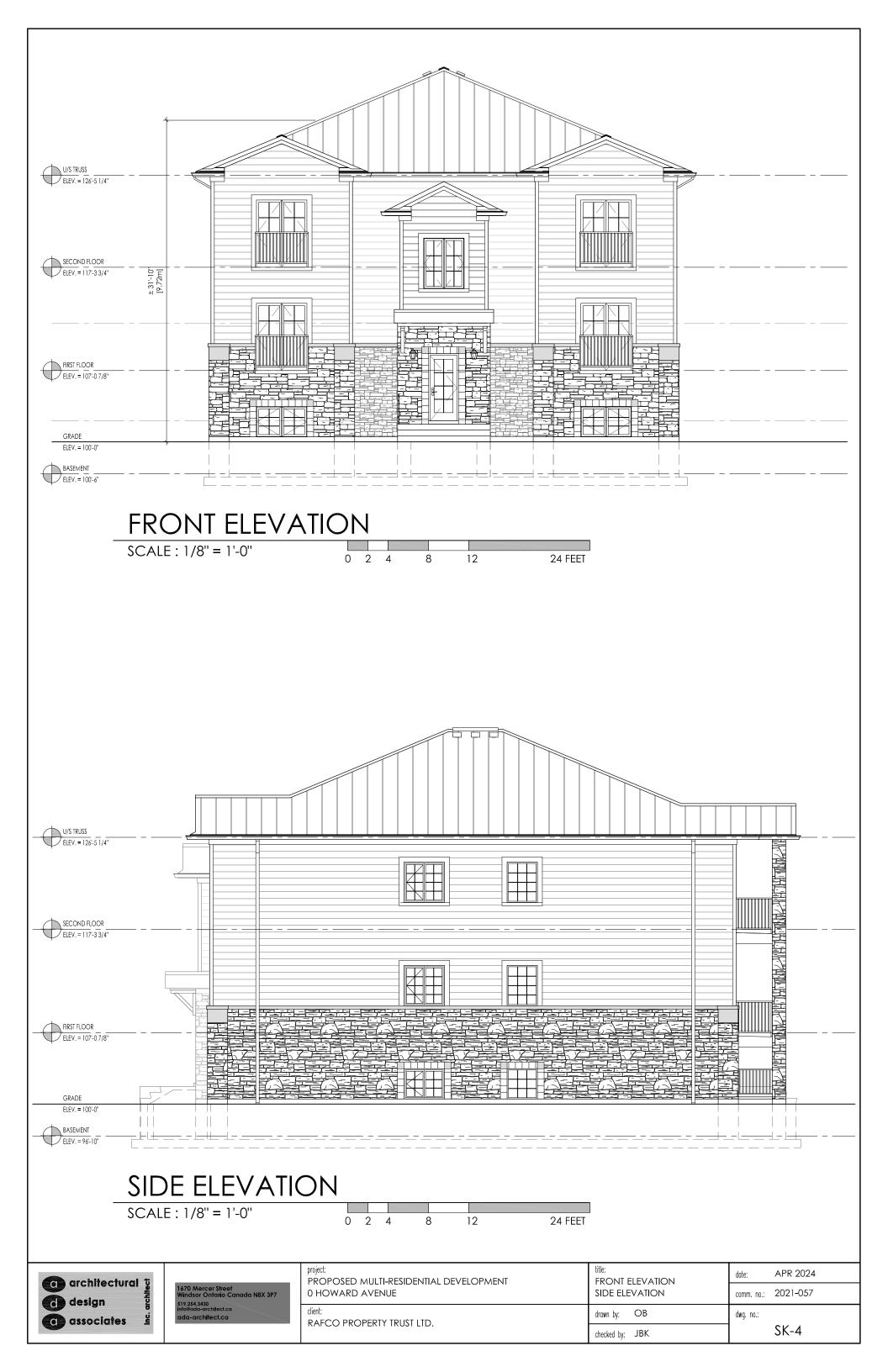


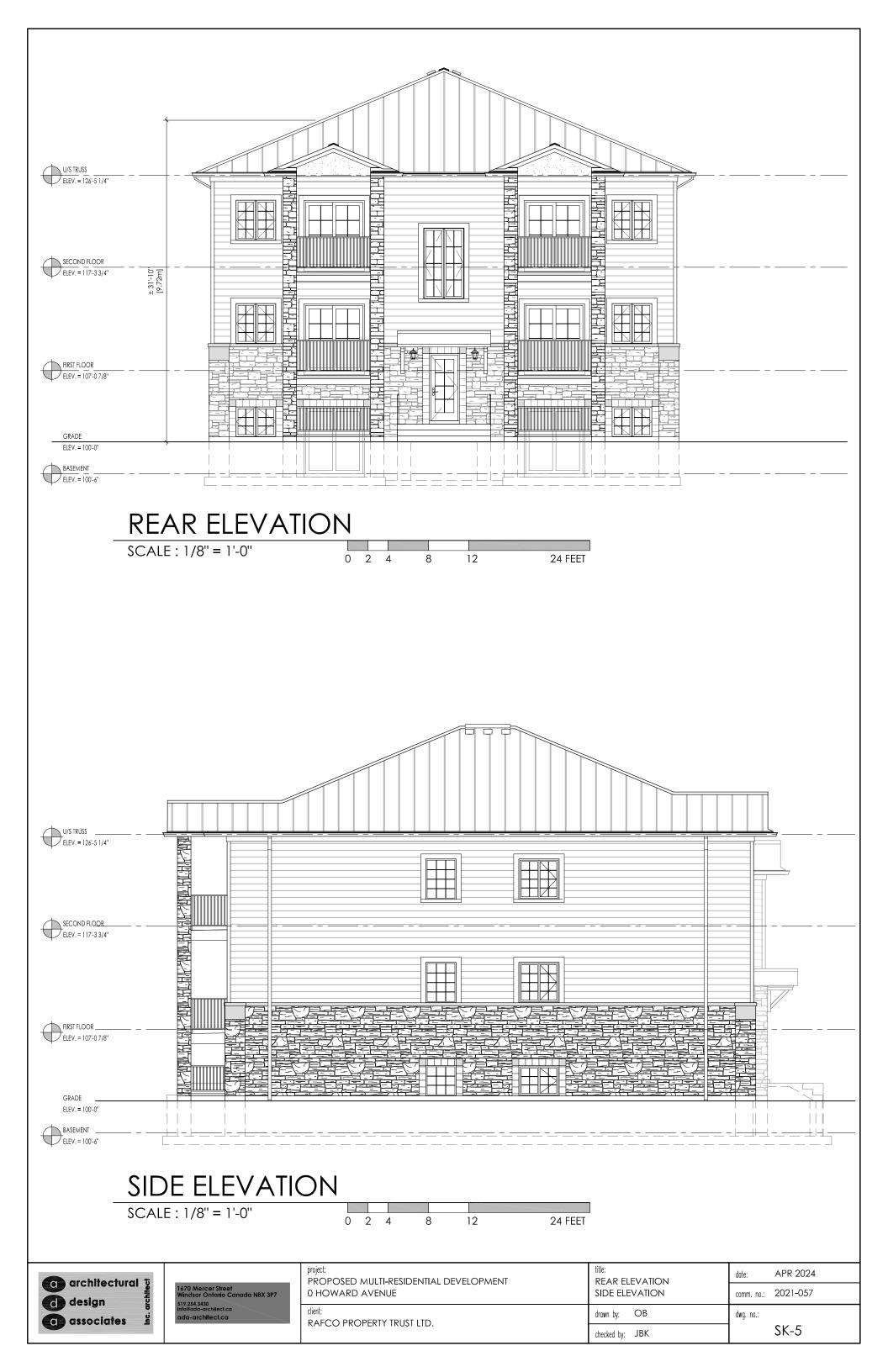


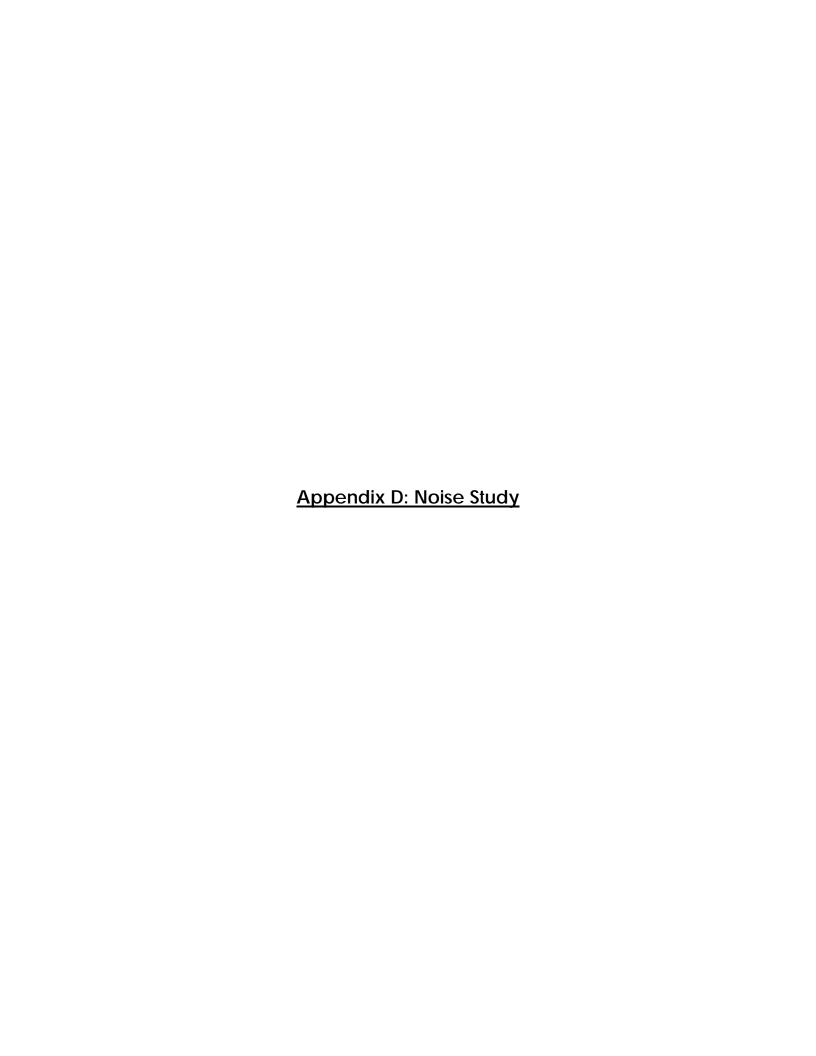
architectural	Hect
design	arch.
associates associates	ij.

1670 Mercer Street Windsor Ontario Canada N8X 3P7 519.254.3430 into@ada-architect.ca ada-architect.ca

project: PROPOSED MULTI-RESIDENTIAL DEVELOPMENT	title: SECOND FLOOR PLAN	date:	APR 2024
0 HOWARD AVENUE		comm. no.:	2021-057
client: RAFCO PROPERTY TRUST LTD.	drawn by: OB	dwg. no.:	
KAICOTROI ERIT IROST EID.	checked by: JBK		SK-3







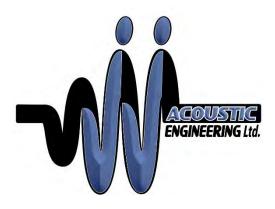


# Road Traffic and Stationary Noise Impact Study

4280 Howard Place, Windsor, Ontario

JJ-00565 NIS1





October 23, 2023

Reference No. JJ-00565-NIS1

OLIVIA BYRNE Junior Project Manager ADA Architects 1670 Mercer St. Windsor, Ontario, N8X 3P7

Dear Ms. Byrne:

Re: Road Traffic and Stationary Noise Impact Study 4280 Howard Place, Windsor, Ontario

#### 1. Introduction

JJ Acoustic Engineering Ltd. (JJAE) was retained to complete a Road Traffic and Stationary Noise Impact Study (Study) for the residential development located at 4280 Howard Place in Windsor, Ontario (Site). The Site will be developed into three 3-storey residential buildings. JJAE has provided a copy of the most up-to-date Site Plan in Attachment A.

The Study was prepared consistent with Ontario Ministry of the Environment, Conservation and Park (MOECP) NPC 300, "Environmental Noise Guideline, Stationary and Transportation Sources—Approval and Planning" dated August 2013.

This Study has determined that the potential environmental noise impact from road traffic noise is significant. The proposed development will need the following: a requirement for central air-conditioning, noise warning clauses and special building components. Road traffic noise control requirements for the Site were determined based on road traffic volumes provided by the City of Windsor (City) and forecasted to 10 years from the date of this study.

The following attachments were included with this Study:

- Attachment A Site Plan
- Attachment B Traffic Data Summary Table & Sample Stamson Traffic Model Outputs
- Attachment C Stationary Noise Impact Figures
- Attachment D Stationary Noise Impact Source Table

#### 2. Road Traffic Analysis

#### 2.1 Road Traffic Noise Modeling Methodology

The road traffic noise impact was conducted using STAMSON, the MOECP's computerized model of ORNAMENT. The Application of the model for the site was consistent with the ORNAMENT technical documents. The computer model input parameters include, among other data, the number of road segments, number of house rows, the positional relationship of the receptor to a noise source or barrier in terms of distance, elevation and angle of exposure to the source, the basic site topography, the ground surface type, traffic volumes, traffic composition and speed limit.

The predicted sound level is based on the 1-hour equivalent sound level, designated as Leq, and is adjusted by the STAMSON program to the 16-hour daytime and the 8-hour nighttime equivalent sound level. The applicable noise criteria for noise sensitive spaces are specified in terms of the 16-hour daytime period (7:00 a.m. to 11:00 p.m.) and 8-hour nighttime period (11:00 p.m. to 7:00 a.m.) enabling a direct comparison between the STAMSON model output and the noise limits.

#### 2.2 Road Traffic Model Input Parameters

This section describes the STAMSON model input parameters used to predict road traffic noise impact for the Site.

The Site has four significant roadways in the vicinity of the development: North Talbot approximately 45 meters to the East of Block A, Howard Avenue approximately 15 meters to the West of Block A, Dougall Parkway East Bound approximately 290 meters to the North of Block A, Dougall Parkway South Bound approximately 300 meters to the North of Block A. Where there are intervening and off-site structures that provide line-of-sight obstruction to the roads, JJAE did not include line-of-sight obstruction in our analysis as to calculate worst-case noise impact.

#### 2.2.1 Road Traffic Parameters

The traffic data provided by the City has been summarized below:

#### North Talbot:

- Current AADT (2012): 8,900
- Forecast AADT (2033): 14,948
- Commercial Vehicle Rates: 2% medium trucks and 3% heavy trucks
- Posted Speed Limit: 50 km/h
- Day Night Splits: 90% day and 10% night

#### Howard Avenue:

- Current AADT (2018): 18,000
- Forecast AADT (2033): 26,069
- Commercial Vehicle Rates: 2% medium trucks and 3% heavy trucks
- Posted Speed Limit: 50 km/h
- Day Night Splits: 90% day and 10% night

#### Dougall Parkway East Bound:

- Current AADT (2019): 12,000
- Forecast AADT (2033): 16,959
- Commercial Vehicle Rates: 2% medium trucks and 3% heavy trucks
- Posted Speed Limit: 60 km/h
- Day Night Splits: 90% day and 10% night

#### Dougall Parkway South Bound:

- Current AADT (2019): 4,600
- Forecast AADT (2033): 6,500
- Commercial Vehicle Rates: 2% medium trucks and 3% heavy trucks
- Posted Speed Limit: 60 km/h
- Day Night Splits: 90% day and 10% night

It should be noted that traffic along Howard Place is 500 AADT, which is considered environmentally insignificant and has not been included in this report.

Moreover, JJAE was not provided with commercial vehicle rates and assumes that medium trucks are 2% and heavy trucks are 3%.

The traffic data is the foundation of this analysis and the Study will be updated if the values change. JJAE assumed 2.5% annual growth to forecast AADT. Traffic data was supplied by the City. The City's AADT report for this Noise Studies report has been supplied in Attachment B.

#### 2.3 Road Traffic Noise Modeling Results

JJAE calculated the Plane of Window (POW) noise exposure for each floor at the Site for the separate daytime and nighttime periods.

The STAMSON road traffic model outputs are provided in Attachment B.

#### 2.4 Road Traffic Modeling Discussion

Noise control requirements will be defined based on NPC 300.

#### Daytime Outdoor Living Area Assessment (NPC 300, Section C7.1.1)

NPC 300 section A5 (pages 13-14) defines an Outdoor Living Area (OLA). As part of this definition, a balcony or terrace is considered an OLA if it has a minimum depth of 4 meters. All balconies are less than 4 m in depth and therefore will not be considered as OLAs.

The OLA is located approximately 10 meters from the East façade of Block C. JJAE has calculated the noise impact to the OLA to be 65dBA. Due to the excess noise level of road traffic, the OLA is not feasible at the location indicated in Attachment A.

#### Plane of a Window – Ventilation Requirements (NPC 300, Section C7.1.2)

The predicted daytime and nighttime Plane of Window (POW) noise impact assumes a worst-case and direct line of sight noise exposure to both roads, unless the building itself blocks line-of-sight (full or partial).

JJAE has used the following criteria, which is a summary of NPC 300 requirements, to evaluate the Site noise impacts from road traffic noise:

Daytime Level (dBA)	Nighttime Level (dBA)	Ventilation Requirements and Warning Clauses	Special Building Components
55	50	Not Required	Not Required
55 – 65	50 – 60	Yes, with Type C Warning Clause	Not Required
66 or more	60 or more	Yes, with Type D Warning Clause	Yes

Table B.1 summarizes the predicted worst-case sound levels and the requirements for the units. The following warning clause is required:

Warning Clause C: "This dwelling unit has been designed with the provision for adding central air conditioning at the occupant's discretion. Installation of central air conditioning by the occupant in low and medium density developments will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment, Conservation and Parks."

Warning Clause D: "This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment"

#### Indoor Living Areas – Building Components (NPC 300, Section C7.1.3)

At minimum, the building must be constructed to standard Ontario Building Code requirements. Improved building components are required and summarized in Table B.1. JJAE has assumed 35% window to floor area coverage and that windows are thick and operable. In addition, exterior wall compositions must be a minimum of STC 46, with brick veneer or masonry equivalent.

### 3. Stationary Noise Impact Analysis

#### 3.1 Stationary Noise Impact Sound Level Criteria

The general criteria for stationary noise sources are defined by NPC 300. The criteria defined in Table C-5 and C-6, "Exclusion Limit Values of One-Hour Equivalent Sound Level (Leq, dBA) Outdoor Points of Reception" and "Exclusion Limit Values of One-Hour Equivalent Sound Level (Leq, dBA) Plane of Window of Noise Sensitive Spaces" are used to evaluate the noise impact at the proposed development.

The criteria for a Class 1 area have been summarized below:

Receiver Category	Time Period	Stationary Noise Criteria
Outdoor Living Area (OLA)	Day = $7:00$ to $23:00$	Leq = 50 dBA
Plane of Window (POW)	Day = $7:00$ to $23:00$	Leq = 50 dBA
	Night = 23:00 to 7:00	Leq = 45 dBA

#### 3.2 Modelling Methodology

The stationary noise impact was evaluated using the CADNA A acoustic modelling software that is based on the ISO 9613-2 standard. The data for all potential stationary noise sources was summarized in Attachment D.

JJAE used the following assumptions in our Cadna A model:

- **Ground Absorption**: Default ground absorption coefficient of 0.7 was used.
- Temperature: 10°C
- Humidity: 70%
- **Building Reflection Coefficient**: Absorption Coefficient Alpha of 0.37 (Reflection Loss of 2dB, Structured Façade) was used.
- **Time-Weighted Adjustment:** where sources operate non-continuously JJAE has provided operating times and as shown in Sections 4 and 5.
- **Tonality**: A 5 dbA tonal penalty was applied to all tonal sources, where applicable. JJAE has provided a (T) for sources identified as tonal in Sections 4 and 5.
- Reflection Order: A maximum reflection order of 1 was used to evaluate indirect noise impact.

## 4. Noise Impact Summary – From Site

The noise from the Site to the neighboring buildings could not be accounted for because the site has not undergone mechanical design yet. An addendum to this report should be completed once a mechanical design is done to account for noise from the Site to the neighboring building.

## 5. Noise Impact Summary – From Environment to Site

There are several buildings near the site. JJAE has identified several potential stationary noise sources including:

#### • Small HVAC Units

A summary of the noise sources used in our modelling is provided in Attachment D.

JJAE modelled the noise impact from all significant noise sources to the Site. The results are summarized in the table below and illustrated on Figure 1.

Block A	Worst Case Daytime Sound Level (dBA)	Daytime Noise Limit (dBA)	Worst Case Nighttime Sound Level (dBA)	Nighttime Noise Limit (dBA)	Limits met
North	30	50	30	45	Yes
East	31	50	31	45	Yes
South	31	50	31	45	Yes
West	<30	50	<30	45	Yes

From the table above it can be seen that all façades are below noise limits.

Block B	Worst Case Daytime Sound Level (dBA)	Daytime Noise Limit (dBA)	Worst Case Nighttime Sound Level (dBA)	Nighttime Noise Limit (dBA)	Limits met
North	31	50	31	45	Yes
East	<30	50	<30	45	Yes
South	<30	50	<30	45	Yes
West	<30	50	<30	45	Yes

From the table above it can be seen that all façades are below noise limits.

Block C	Worst Case Daytime Sound Level (dBA)	Daytime Noise Limit (dBA)	Worst Case Nighttime Sound Level (dBA)	Nighttime Noise Limit (dBA)	Limits met
North	32	50	32	45	Yes
East	32	50	32	45	Yes
South	<30	50	<30	45	Yes
West	<30	50	<30	45	Yes

From the table above it can be seen that all façades are below noise limits.

#### 6. Recommendations

The road traffic noise impacts were above the NPC 300 requirements. Noise mitigation measures include:

#### Block A:

- Warning Clause Type C for the North and East façades.
- Warning Clause Type D for the South and West façades.
- A minimum of STC 35 is required for all exterior glazing for the West façade.
- A minimum of STC 32 is required for all exterior glazing for the South façade.
- JJAE and the client require air conditioning for all units.

#### Block B:

- Warning Clause Type C for all façades.
- JJAE and the client require air conditioning for all units.

#### **Block C:**

- Warning Clause Type C for all façades.
- JJAE and the client require air conditioning for all units.

#### **Outdoor Living Area (OLA):**

• Due to the excess noise level of road traffic, the OLA is not feasible at the location indicated in Attachment A.

The stationary noise impacts from neighboring buildings to the site were evaluated and the sound level predictions were determined to be below noise limits.

The noise from the Site to the neighboring buildings could not be accounted for because the site has not undergone mechanical design yet. An addendum to this report should be completed once a mechanical design is done to account for noise from the Site to the neighboring building.

#### 7. Conclusions

The results of this Study indicate that the potential environmental impact from road traffic sources are significant. Mitigation measures will be required including ventilation requirements, special building components and noise warning clauses for each unit. With the mitigation measures, provided in Section 6.

Should you have any questions on the above, please do not hesitate to contact us.

Yours truly,

Written By: Reviewed by:

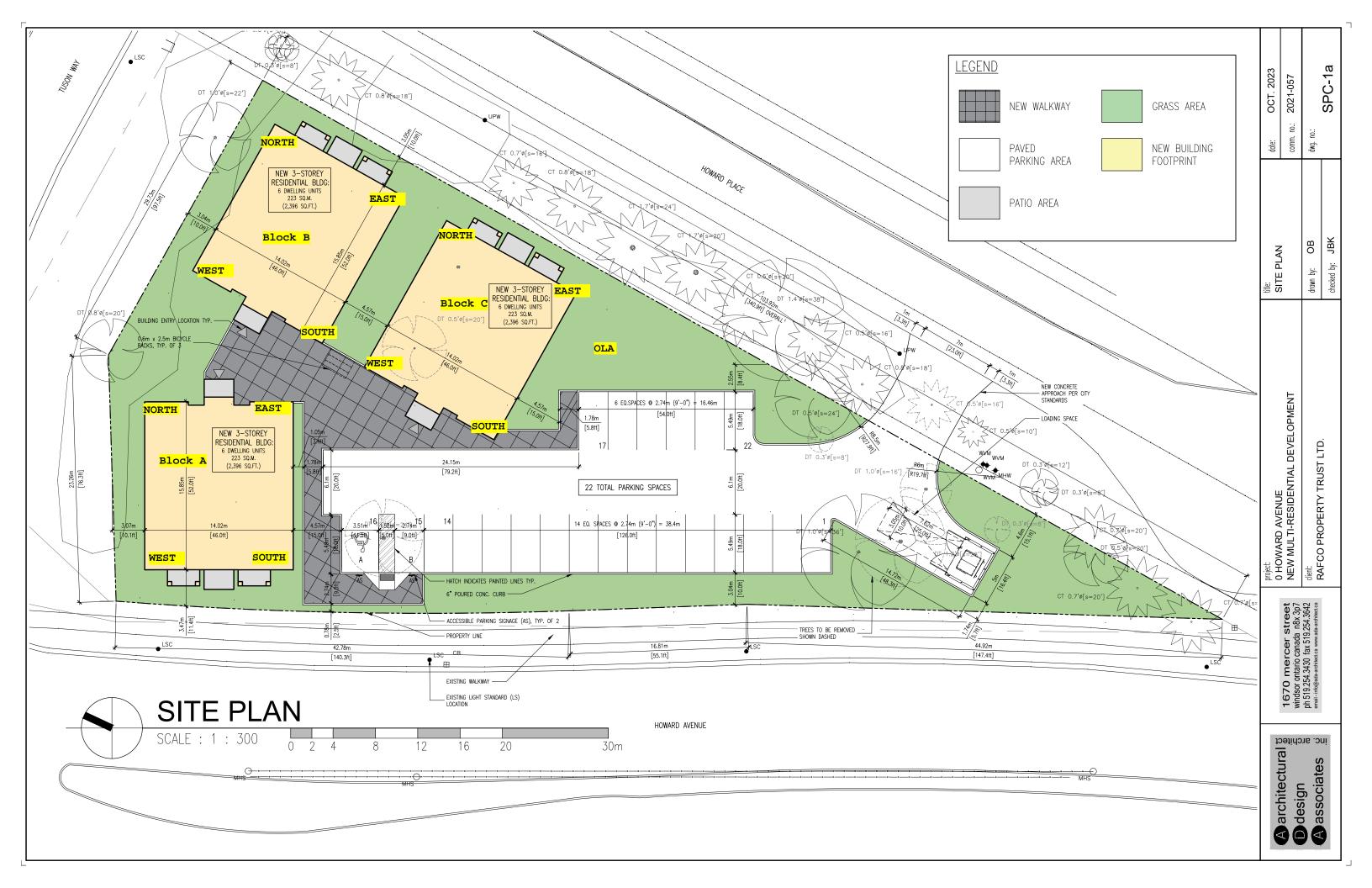
Oct. 23, 2023

Joseph Sleiman Acoustic Technician

Joseph Heimin.

Joey Jraige, P.Eng., B.A.Sc. President (Owner)





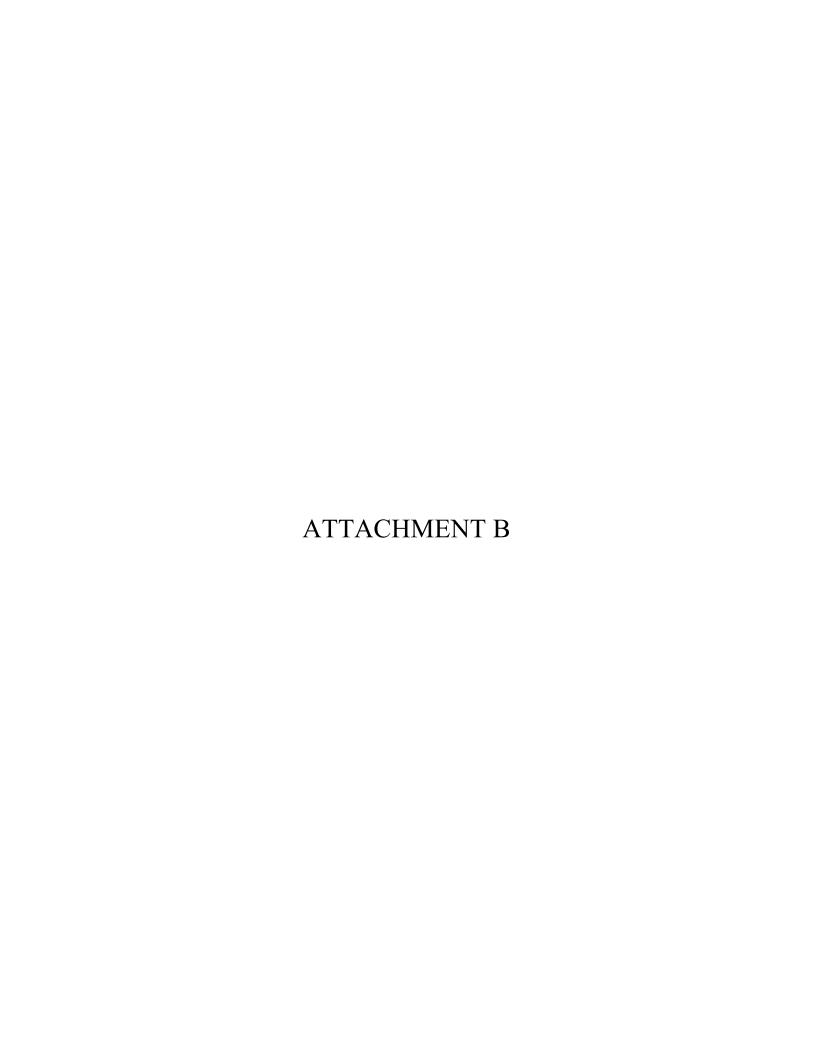


Table B1

Road Traffic Noise Levels and Mitigation Measures Summary
4280 Howard Place Block A, Windsor, Ontario

	<b>Road Sound Level</b>	<b>Road Sound Level</b>		Warning Clauses	
Point of Reception	Daytime (dBA)	Nighttime (dBA)	Ventilation Requirements NPC 300	From NPC 300	Special Building Components
North Façade					
Plane of Window Level 1	64 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	64 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	64 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
East Façade					
Plane of Window Level 1	60 (dBA)	53 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	60 (dBA)	53 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	60 (dBA)	53 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
South Façade					
Plane of Window Level 1	66 (dBA)	60 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 32
Plane of Window Level 2	66 (dBA)	59 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 32
Plane of Window Level 3	66 (dBA)	59 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 32
West Façade					
Plane of Window Level 1	69 (dBA)	62 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 35
Plane of Window Level 2	69 (dBA)	62 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 35
Plane of Window Level 3	68 (dBA)	62 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 34

Table B1

Road Traffic Noise Levels and Mitigation Measures Summary
4280 Howard Place Block B, Windsor, Ontario

	<b>Road Sound Level</b>	<b>Road Sound Level</b>		Warning Clauses	
Point of Reception	Daytime (dBA)	Nighttime (dBA)	Ventilation Requirements NPC 300	From NPC 300	<b>Special Building Components</b>
North Façade					
Plane of Window Level 1	62 (dBA)	55 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	62 (dBA)	55 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	62 (dBA)	55 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
East Façade					
Plane of Window Level 1	57 (dBA)	50 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	57 (dBA)	50 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	57 (dBA)	50 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
South Façade					
Plane of Window Level 1	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
West Façade					
Plane of Window Level 1	65 (dBA)	59 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	65 (dBA)	59 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	65 (dBA)	59 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code

Table B1

Road Traffic Noise Levels and Mitigation Measures Summary
4280 Howard Place Block C, Windsor, Ontario

Data of Daniella	Road Sound Level	Road Sound Level	V41-4: D:	Warning Clauses	Constal Building Common and
Point of Reception	Daytime (dBA)	Nighttime (dBA)	Ventilation Requirements NPC 300	From NPC 300	Special Building Components
North Façade					
Plane of Window Level 1	61 (dBA)	55 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	61 (dBA)	55 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	61 (dBA)	55 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
East Façade					
Plane of Window Level 1	57 (dBA)	50 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	57 (dBA)	50 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	57 (dBA)	50 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
South Façade					
Plane of Window Level 1	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
West Façade					
Plane of Window Level 1	65 (dBA)	59 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	65 (dBA)	59 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	65 (dBA)	59 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Outdoor Living Area					
OLA	65 (dBA)	N/A	N/A		N/A

### Joseph Sleiman

From: Spagnuolo, Mike <mspagnuolo@citywindsor.ca>

Sent: Wednesday, August 23, 2023 10:55 AM

**To:** Joey Jraige; Joseph Sleiman; Amicarelli, Clare; Dhiman, Siddharth **Subject:** RE: Traffic Data for surrounding roadways 4280 Howard Avenue

Joey, here is the information I have; Howard Place north of Tuson Way 500 (2018) Howard Ave north of North Talbot 18,000 (2018) North Talbot East of Howard 8,900 (2012) Dougall Parkway Eastbound east of Howard ramps 12,000 (2019)

Dougall Parkway to Southbound Howard off ramp 4,600 (2019)

MIKE SPAGNUOLO | SIGNAL SYSTEMS ANALYST

WINDSOR ONTARIO, CANADA

Office Of The City Engineer 1269 Mercer St | Windsor, ON | N8X 0A9 (519) 255-6247 Ext 6061

www.citywindsor.ca

From: Joey Jraige <joey@jjae.ca>
Sent: August 23, 2023 8:53 AM

To: Spagnuolo, Mike <mspagnuolo@citywindsor.ca>; Joseph Sleiman <Joseph@jjae.ca>; Amicarelli, Clare

<CAmicarelli@citywindsor.ca>; Dhiman, Siddharth <SDhiman@citywindsor.ca> **Subject:** Re: Traffic Data for surrounding roadways 4280 Howard Avenue

**CAUTION**: This email originated from outside of the organization. Do not click links or open attachments unless you recognize the sender and know the content is safe.

Hello Mike,

The address is 4280 Howard Place

Regards,

Joey Jraige JJ Acoustic Engineering Ltd. 226-346-6473

joey@jjae.ca

From: Spagnuolo, Mike < mspagnuolo@citywindsor.ca>

Sent: Wednesday, August 23, 2023 8:24:23 AM

To: Joseph Sleiman < <u>Joseph@jjae.ca</u>>; Amicarelli, Clare < <u>CAmicarelli@citywindsor.ca</u>>; Dhiman, Siddharth

<<u>SDhiman@citywindsor.ca</u>>
Cc: Joey Jraige <<u>joey@jjae.ca</u>>

Subject: RE: Traffic Data for surrounding roadways 4280 Howard Avenue

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:06:39

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b1north.te Time Period: Day/Night 16/8 hours

Description: Building #1 North Facade Floor 1

Road data, segment # 1: Howard Ave (day/night)

-----

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000
Percentage of Annual Growth : 2.50
Number of Years of Growth : 15.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Howard Ave (day/night)

-----

Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 29.00 / 29.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Dougal Pk Ea (day/night)

-----

Car traffic volume : 14497/1611 veh/TimePeriod \*
Medium truck volume : 305/34 veh/TimePeriod \*
Heavy truck volume : 458/51 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 2.50

Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 2: Dougal Pk Ea (day/night) -----Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface) Receiver source distance : 290.00 / 290.00 m Receiver height : 2.00 / 2.00 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle : 0.00 Road data, segment # 3: Dougal Pk So (day/night) \_\_\_\_\_ Car traffic volume : 5557/617 veh/TimePeriod \* Medium truck volume : 117/13 veh/TimePeriod \* Heavy truck volume : 175/19 veh/TimePeriod \* Posted speed limit : 60 km/h Road gradient : Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 4600 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 3: Dougal Pk So (day/night) Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods Wood depth : 0
No of house rows : 0 / 0
Surface : 2 (No woods.) 2 Surface (Reflective ground surface) Receiver source distance : 300.00 / 300.00 m

: 1 (Flat/gentle slope; no barrier)

Results segment # 1: Howard Ave (day)

Reference angle : 0.00

Topography

Receiver height : 2.00 / 2.00

ROAD (0.00 + 62.83 + 0.00) = 62.83 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq - 90 0 0.00 68.71 0.00 - 2.86 - 3.01 0.00 0.00 0.00 62.83

\_\_\_\_\_\_

Segment Leq: 62.83 dBA

Results segment # 2: Dougal Pk Ea (day)

Source height = 1.32 m

ROAD (0.00 + 55.56 + 0.00) = 55.56 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 68.42 0.00 -12.86 0.00 0.00 0.00 0.00 55.56

Segment Leq: 55.56 dBA

Results segment # 3: Dougal Pk So (day)

Source height = 1.32 m

ROAD (0.00 + 51.24 + 0.00) = 51.24 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 64.25 0.00 -13.01 0.00 0.00 0.00 0.00 51.24

Segment Leq: 51.24 dBA

Total Leq All Segments: 63.82 dBA

Results segment # 1: Howard Ave (night)

Source height = 1.32 m

Segment Leq : 56.29 dBA

Results segment # 2: Dougal Pk Ea (night)

-----

Source height = 1.32 m

ROAD (0.00 + 49.03 + 0.00) = 49.03 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 61.89 0.00 -12.86 0.00 0.00 0.00 0.00 49.03

Segment Leq: 49.03 dBA

Results segment # 3: Dougal Pk So (night)

\_\_\_\_\_

Source height = 1.31 m

ROAD (0.00 + 44.65 + 0.00) = 44.65 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 57.66 0.00 -13.01 0.00 0.00 0.00 0.00 44.65

-----

Segment Leq: 44.65 dBA

Total Leq All Segments: 57.28 dBA

TOTAL Leg FROM ALL SOURCES (DAY): 63.82

(NIGHT): 57.28

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:07:22

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b1east.te Time Period: Day/Night 16/8 hours

Description: Building #1 East Facade Floor 1

Road data, segment # 1: North Talbot (day/night)

Car traffic volume : 12781/1420 veh/TimePeriod \*
Medium truck volume : 269/30 veh/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 45.00 / 45.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Dougal Pk Ea (day/night)

-----

Car traffic volume : 14497/1611 veh/TimePeriod \*
Medium truck volume : 305/34 veh/TimePeriod \*
Heavy truck volume : 458/51 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 2.50

Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 2: Dougal Pk Ea (day/night) -----Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective (Reflective ground surface) Receiver source distance : 295.00 / 295.00 m Receiver height : 2.00 / 2.00 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle : 0.00 Road data, segment # 3: Dougal Pk So (day/night) \_\_\_\_\_ Car traffic volume : 5557/617 veh/TimePeriod \* Medium truck volume : 117/13 veh/TimePeriod \* Heavy truck volume : 175/19 veh/TimePeriod \* Posted speed limit : 60 km/h Road gradient : Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 4600 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 3: Dougal Pk So (day/night) Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 (No woods Wood depth : 0
No of house rows : 0 / 0
Surface : 2 (No woods.) 0 / 0

2

(Reflective ground surface)

: 1 (Flat/gentle slope; no barrier)

Results segment # 1: North Talbot (day)

Reference angle : 0.00

Receiver source distance : 305.00 / 305.00 m Receiver height : 2.00 / 2.00

Surface

Topography

ROAD (0.00 + 58.51 + 0.00) = 58.51 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 66.29 0.00 - 4.77 - 3.01 0.00 0.00 0.00 58.51

Segment Leq: 58.51 dBA

Results segment # 2: Dougal Pk Ea (day)

Source height = 1.32 m

ROAD (0.00 + 52.47 + 0.00) = 52.47 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

Segment Leq: 52.47 dBA

Results segment # 3: Dougal Pk So (day)

-----

Source height = 1.32 m

ROAD (0.00 + 48.15 + 0.00) = 48.15 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

Segment Leq: 48.15 dBA

Total Leq All Segments: 59.78 dBA

Results segment # 1: North Talbot (night)

-----

Source height = 1.32 m

ROAD (0.00 + 51.99 + 0.00) = 51.99 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 59.77 0.00 - 4.77 - 3.01 0.00 0.00 0.00 51.99

Segment Leq : 51.99 dBA

Results segment # 2: Dougal Pk Ea (night)

Source height = 1.32 m

ROAD (0.00 + 45.95 + 0.00) = 45.95 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

Segment Leq: 45.95 dBA

Results segment # 3: Dougal Pk So (night)

Source height = 1.31 m

ROAD (0.00 + 41.57 + 0.00) = 41.57 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_\_

Segment Leq: 41.57 dBA

Total Leq All Segments: 53.26 dBA

TOTAL Leg FROM ALL SOURCES (DAY): 59.78

(NIGHT): 53.26

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:07:02

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b1south.te Time Period: Day/Night 16/8 hours

Description: Building #1 South Facade Floor 1

Road data, segment # 1: North Talbot (day/night)

Car traffic volume : 12781/1420 veh/TimePeriod \*
Medium truck volume : 269/30 veh/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 140.00 / 140.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Howard Ave (day/night)

-----

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000 Percentage of Annual Growth : 2.50 Number of Years of Growth : 15.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 2: Howard Ave (day/night)

-----

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 15.00 / 15.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: North Talbot (day)

-----

Source height = 1.32 m

ROAD (0.00 + 56.59 + 0.00) = 56.59 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 66.29 0.00 - 9.70 0.00 0.00 0.00 0.00 56.59

------

Segment Leq: 56.59 dBA

Results segment # 2: Howard Ave (day)

-----

Source height = 1.32 m

ROAD (0.00 + 65.70 + 0.00) = 65.70 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 68.71 0.00 0.00 - 3.01 0.00 0.00 0.00 65.70

\_\_\_\_\_\_

Segment Leq: 65.70 dBA

Total Leq All Segments: 66.20 dBA

Results segment # 1: North Talbot (night)

-----

ROAD (0.00 + 50.07 + 0.00) = 50.07 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
- 90 90 0.00 59.77 0.00 - 9.70 0.00 0.00 0.00 0.00 50.07

Segment Leq: 50.07 dBA

Results segment # 2: Howard Ave (night)

Source height = 1.32 m

ROAD (0.00 + 59.16 + 0.00) = 59.16 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 62.17 0.00 0.00 - 3.01 0.00 0.00 0.00 59.16

Segment Leq: 59.16 dBA

Total Leq All Segments: 59.66 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 66.20 (NIGHT): 59.66

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:07:37

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b1west.te Time Period: Day/Night 16/8 hours

Description: Building #1 West Facade Floor 1

Road data, segment # 1: North Talbot (day/night)

Car traffic volume : 12781/1420 veh/TimePeriod \*

Medium truck volume : 269/30 veh/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 152.00 / 152.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Howard Ave (day/night)

-----

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000 Percentage of Annual Growth : 2.50

Number of Years of Growth : 15.00 Medium Truck % of Total Volume : 2.00 Heavy Truck % of Total Volume : 3.00 Day (16 hrs) % of Total Volume : 90.00

#### Data for Segment # 2: Howard Ave (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth .
No of house rows : (No woods.) : 0

0 / 0

2 (Reflective ground surface)

Receiver source distance : 15.00 / 15.00 m Receiver height : 2.00 / 2.00

: 1 (Flat/gentle slope; no barrier) Topography

Reference angle : 0.00

# Road data, segment # 3: Dougal Pk Ea (day/night)

Car traffic volume : 14497/1611 veh/TimePeriod \* Medium truck volume: 305/34 veh/TimePeriod \* Heavy truck volume : 458/51 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

: 1 (Typical asphalt or concrete) Road pavement

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00 Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

### Data for Segment # 3: Dougal Pk Ea (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth 0 (No woods.) Wood depth
No of house rows

0 / 0

Surface 2 (Reflective ground surface)

Receiver source distance : 295.00 / 295.00 m Receiver height : 2.00 / 2.00 m

(Flat/gentle slope; no barrier) Topography 1

Reference angle : 0.00

Road data, segment # 4: Dougal Pk So (day/night)

-----

Car traffic volume : 5557/617 veh/TimePeriod \*

Medium truck volume : 117/13 veh/TimePeriod \* Heavy truck volume : 175/19 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4600 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00 Number of Years of Growth : 14.00 Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 4: Dougal Pk So (day/night) -----

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth :
No of house rows : : 0 (No woods.)

0 / 0

: 2 (Reflective ground surface)

Receiver source distance : 305.00 / 305.00 m Receiver height : 2.00 / 2.00 m

: 1 (Flat/gentle slope; no barrier) Topography

Reference angle : 0.00

Results segment # 1: North Talbot (day) -----

Source height = 1.32 m

ROAD (0.00 + 53.23 + 0.00) = 53.23 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ 0 90 0.00 66.29 0.00 -10.06 - 3.01 0.00 0.00 0.00 53.23 -----

Segment Leq: 53.23 dBA

Results segment # 2: Howard Ave (day) -----

Source height = 1.32 m

ROAD (0.00 + 68.71 + 0.00) = 68.71 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ - 90 90 0.00 68.71 0.00 0.00 0.00 0.00 0.00 0.00 68.71

.-----

Segment Leq : 68.71 dBA

Results segment # 3: Dougal Pk Ea (day)

Source height = 1.32 m

ROAD (0.00 + 52.47 + 0.00) = 52.47 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 68.42 0.00 -12.94 - 3.01 0.00 0.00 0.00 52.47

Segment Leq: 52.47 dBA

Results segment # 4: Dougal Pk So (day)

-----

Source height = 1.32 m

ROAD (0.00 + 48.15 + 0.00) = 48.15 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 64.25 0.00 -13.08 - 3.01 0.00 0.00 0.00 48.15

Segment Leq : 48.15 dBA

Total Leq All Segments: 68.97 dBA

Results segment # 1: North Talbot (night)

-----

Source height = 1.32 m

ROAD (0.00 + 46.70 + 0.00) = 46.70 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 59.77 0.00 -10.06 - 3.01 0.00 0.00 0.00 46.70

Segment Leq: 46.70 dBA

Results segment # 2: Howard Ave (night)

ROAD (0.00 + 62.17 + 0.00) = 62.17 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ - 90 90 0.00 62.17 0.00 0.00 0.00 0.00 0.00 62.17 \_\_\_\_\_\_

Segment Leq: 62.17 dBA

Results segment # 3: Dougal Pk Ea (night) -----

Source height = 1.32 m

ROAD (0.00 + 45.95 + 0.00) = 45.95 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ 90 0.00 61.89 0.00 -12.94 - 3.01 0.00 0.00 0.00 45.95 \_\_\_\_\_\_

Segment Leq: 45.95 dBA

Results segment # 4: Dougal Pk So (night) \_\_\_\_\_

Source height = 1.31 m

ROAD (0.00 + 41.57 + 0.00) = 41.57 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ 0 90 0.00 57.66 0.00 -13.08 - 3.01 0.00 0.00 0.00 41.57 \_\_\_\_\_\_

Segment Leq: 41.57 dBA

Total Leq All Segments: 62.43 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 68.97

(NIGHT): 62.43

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:08:23

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b2north.te Time Period: Day/Night 16/8 hours

Description: Building #2 North Facade Floor 1

Road data, segment # 1: Howard Ave (day/night)

-----

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000
Percentage of Annual Growth : 2.50
Number of Years of Growth : 15.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Howard Ave (day/night)

-----

Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 60.00 / 60.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Dougal Pk Ea (day/night)

-----

Car traffic volume : 14497/1611 veh/TimePeriod \*
Medium truck volume : 305/34 veh/TimePeriod \*
Heavy truck volume : 458/51 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 2.50

Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 2: Dougal Pk Ea (day/night) -----Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface) Receiver source distance : 290.00 / 290.00 m Receiver height : 2.00 / 2.00 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle : 0.00 Road data, segment # 3: Dougal Pk So (day/night) \_\_\_\_\_ Car traffic volume : 5557/617 veh/TimePeriod \* Medium truck volume : 117/13 veh/TimePeriod \* Heavy truck volume : 175/19 veh/TimePeriod \* Posted speed limit : 60 km/h Road gradient : Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 4600 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 3: Dougal Pk So (day/night) Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods Wood depth : 0
No of house rows : 0 / 0
Surface : 2 (No woods.) 2 Surface (Reflective ground surface) Receiver source distance : 300.00 / 300.00 m

: 1 (Flat/gentle slope; no barrier)

Results segment # 1: Howard Ave (day)

Reference angle : 0.00

Topography

Receiver height : 2.00 / 2.00

Segment Leq: 59.68 dBA

Results segment # 2: Dougal Pk Ea (day)

Source height = 1.32 m

ROAD (0.00 + 55.56 + 0.00) = 55.56 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 68.42 0.00 -12.86 0.00 0.00 0.00 0.00 55.56

Segment Leq: 55.56 dBA

Results segment # 3: Dougal Pk So (day)

Source height = 1.32 m

ROAD (0.00 + 51.24 + 0.00) = 51.24 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 64.25 0.00 -13.01 0.00 0.00 0.00 0.00 51.24

Segment Leq: 51.24 dBA

Total Leq All Segments: 61.53 dBA

Results segment # 1: Howard Ave (night)

Source height = 1.32 m

Segment Leq : 53.14 dBA

Results segment # 2: Dougal Pk Ea (night)

Source height = 1.32 m

ROAD (0.00 + 49.03 + 0.00) = 49.03 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 61.89 0.00 -12.86 0.00 0.00 0.00 0.00 49.03

Segment Leq: 49.03 dBA

Results segment # 3: Dougal Pk So (night)

-----

Source height = 1.31 m

ROAD (0.00 + 44.65 + 0.00) = 44.65 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 57.66 0.00 -13.01 0.00 0.00 0.00 0.00 44.65

-----

Segment Leq: 44.65 dBA

Total Leq All Segments: 54.99 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 61.53

(NIGHT): 54.99

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:08:57

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b2east.te Time Period: Day/Night 16/8 hours

Description: Building #2 East Facade Floor 1

Road data, segment # 1: North Talbot (day/night)

Car traffic volume : 12781/1420 veh/TimePeriod \*

Medium truck volume : 12/81/1420 ven/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0/0

Surface : 2 (Reflective ground surface)

Receiver source distance : 145.00 / 145.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Dougal Pk Ea (day/night)

-----

Car traffic volume : 14497/1611 veh/TimePeriod \*
Medium truck volume : 305/34 veh/TimePeriod \*
Heavy truck volume : 458/51 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 2.50

Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 2: Dougal Pk Ea (day/night) -----Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective (Reflective ground surface) Receiver source distance : 295.00 / 295.00 m Receiver height : 2.00 / 2.00 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle : 0.00 Road data, segment # 3: Dougal Pk So (day/night) \_\_\_\_\_ Car traffic volume : 5557/617 veh/TimePeriod \* Medium truck volume : 117/13 veh/TimePeriod \* Heavy truck volume : 175/19 veh/TimePeriod \* Posted speed limit : 60 km/h Road gradient : Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 4600 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 3: Dougal Pk So (day/night) Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 (No woods Wood depth : 0
No of house rows : 0 / 0
Surface : 2 (No woods.) 0 / 0

2

(Reflective ground surface)

: 1 (Flat/gentle slope; no barrier)

Results segment # 1: North Talbot (day)

Reference angle : 0.00

Receiver source distance : 305.00 / 305.00 m Receiver height : 2.00 / 2.00

Surface

Topography

ROAD (0.00 + 53.43 + 0.00) = 53.43 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 66.29 0.00 - 9.85 - 3.01 0.00 0.00 0.00 53.43

-----

Segment Leq: 53.43 dBA

Results segment # 2: Dougal Pk Ea (day)

-----

Source height = 1.32 m

ROAD (0.00 + 52.47 + 0.00) = 52.47 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_

Segment Leq : 52.47 dBA

Results segment # 3: Dougal Pk So (day)

-----

Source height = 1.32 m

ROAD (0.00 + 48.15 + 0.00) = 48.15 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 30 0 0.00 04.23 0.00 -13.00 - 3.01 0.00 0.00 0.00 40.13

Segment Leq: 48.15 dBA

Total Leq All Segments: 56.65 dBA

Results segment # 1: North Talbot (night)

-----

Source height = 1.32 m

ROAD (0.00 + 46.91 + 0.00) = 46.91 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 59.77 0.00 - 9.85 - 3.01 0.00 0.00 0.00 46.91

-----

Segment Leq: 46.91 dBA

Results segment # 2: Dougal Pk Ea (night)

-----

Source height = 1.32 m

ROAD (0.00 + 45.95 + 0.00) = 45.95 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

Segment Leq: 45.95 dBA

Results segment # 3: Dougal Pk So (night)

\_\_\_\_\_

Source height = 1.31 m

ROAD (0.00 + 41.57 + 0.00) = 41.57 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_\_

Segment Leq: 41.57 dBA

Total Leq All Segments: 50.12 dBA

TOTAL Leg FROM ALL SOURCES (DAY): 56.65

(NIGHT): 50.12

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:08:39

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b2south.te Time Period: Day/Night 16/8 hours

Description: Building #2 South Facade Floor 1

Road data, segment # 1: North Talbot (day/night)

Can thatfic valuma : 12791/1420 vah/TimaDaniad

Car traffic volume : 12781/1420 veh/TimePeriod \*
Medium truck volume : 269/30 veh/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 146.00 / 146.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Howard Ave (day/night)

-----

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000 Percentage of Annual Growth : 2.50 Number of Years of Growth : 15.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 2: Howard Ave (day/night)

-----

: 0.00 deg 90.00 deg : 0 (No woods Angle1 Angle2 Wood depth (No woods.)

No of house rows : 0 / 0

2 (Reflective ground surface) Surface

Receiver source distance : 34.00 / 34.00 m Receiver height : 2.00 / 2.00 m

: 1 (Flat/gentle slope; no barrier) Topography

: 0.00 Reference angle

Results segment # 1: North Talbot (day) \_\_\_\_\_

Source height = 1.32 m

ROAD (0.00 + 56.41 + 0.00) = 56.41 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ - 90 90 0.00 66.29 0.00 - 9.88 0.00 0.00 0.00 0.00 56.41

------

Segment Leq: 56.41 dBA

Results segment # 2: Howard Ave (day)

\_\_\_\_\_

Source height = 1.32 m

ROAD (0.00 + 62.14 + 0.00) = 62.14 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_

0 90 0.00 68.71 0.00 - 3.55 - 3.01 0.00 0.00 0.00 62.14

\_\_\_\_\_\_

Segment Leq: 62.14 dBA

Total Leq All Segments: 63.17 dBA

Results segment # 1: North Talbot (night)

Segment Leq: 49.89 dBA

Results segment # 2: Howard Ave (night)

Source height = 1.32 m

ROAD (0.00 + 55.60 + 0.00) = 55.60 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 62.17 0.00 - 3.55 - 3.01 0.00 0.00 0.00 55.60

Segment Leq: 55.60 dBA

Total Leq All Segments: 56.63 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 63.17 (NIGHT): 56.63

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:09:15

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b2west.te Time Period: Day/Night 16/8 hours

Description: Building #2 West Facade Floor 1

Road data, segment # 1: North Talbot (day/night)

-----

Car traffic volume : 12781/1420 veh/TimePeriod \*
Medium truck volume : 269/30 veh/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 160.00 / 160.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Howard Ave (day/night)

-----

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000 Percentage of Annual Growth : 2.50

Number of Years of Growth : 15.00 Medium Truck % of Total Volume : 2.00 Heavy Truck % of Total Volume : 3.00 Day (16 hrs) % of Total Volume : 90.00

#### Data for Segment # 2: Howard Ave (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth (No woods.) : 0

No of house rows : 0 / 0

2 Surface (Reflective ground surface)

Receiver source distance : 39.00 / 39.00 m Receiver height : 2.00 / 2.00

: 1 (Flat/gentle slope; no barrier) Topography

Reference angle : 0.00

# Road data, segment # 3: Dougal Pk Ea (day/night)

Car traffic volume : 14497/1611 veh/TimePeriod \* Medium truck volume: 305/34 veh/TimePeriod \* Heavy truck volume : 458/51 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

: 1 (Typical asphalt or concrete) Road pavement

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00 Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

## Data for Segment # 3: Dougal Pk Ea (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth 0 (No woods.) Wood depth
No of house rows

0 / 0

Surface 2 (Reflective ground surface)

Receiver source distance : 295.00 / 295.00 m Receiver height : 2.00 / 2.00 m

(Flat/gentle slope; no barrier) Topography 1

Reference angle : 0.00

Road data, segment # 4: Dougal Pk So (day/night)

-----

Car traffic volume : 5557/617 veh/TimePeriod \*

Medium truck volume : 117/13 veh/TimePeriod \* Heavy truck volume : 175/19 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4600
Percentage of Annual Growth : 2.50
Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 4: Dougal Pk So (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.)

Wood depth : 0
No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 305.00 / 305.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: North Talbot (day)

Source height = 1.32 m

ROAD (0.00 + 53.00 + 0.00) = 53.00 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 66.29 0.00 -10.28 - 3.01 0.00 0.00 0.00 53.00

Segment Leq: 53.00 dBA

Results segment # 2: Howard Ave (day)

Source height = 1.32 m

Segment Leq : 64.56 dBA

Results segment # 3: Dougal Pk Ea (day)

Source height = 1.32 m

ROAD (0.00 + 52.47 + 0.00) = 52.47 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 68.42 0.00 -12.94 - 3.01 0.00 0.00 0.00 52.47

Segment Leq: 52.47 dBA

Results segment # 4: Dougal Pk So (day)

-----

Source height = 1.32 m

ROAD (0.00 + 48.15 + 0.00) = 48.15 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 64.25 0.00 -13.08 - 3.01 0.00 0.00 0.00 48.15

.....

Segment Leq: 48.15 dBA

Total Leq All Segments: 65.18 dBA

Results segment # 1: North Talbot (night)

-----

Source height = 1.32 m

ROAD (0.00 + 46.48 + 0.00) = 46.48 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 59.77 0.00 -10.28 - 3.01 0.00 0.00 0.00 46.48

Segment Leq: 46.48 dBA

Results segment # 2: Howard Ave (night)

ROAD (0.00 + 58.02 + 0.00) = 58.02 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ - 90 90 0.00 62.17 0.00 - 4.15 0.00 0.00 0.00 0.00 58.02

Segment Leq: 58.02 dBA

Results segment # 3: Dougal Pk Ea (night) -----

Source height = 1.32 m

ROAD (0.00 + 45.95 + 0.00) = 45.95 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ 90 0.00 61.89 0.00 -12.94 - 3.01 0.00 0.00 0.00 45.95 \_\_\_\_\_\_

Segment Leq: 45.95 dBA

Results segment # 4: Dougal Pk So (night) \_\_\_\_\_

Source height = 1.31 m

ROAD (0.00 + 41.57 + 0.00) = 41.57 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ 90 0.00 57.66 0.00 -13.08 - 3.01 0.00 0.00 0.00 41.57 \_\_\_\_\_\_

Segment Leq: 41.57 dBA

Total Leq All Segments: 58.65 dBA

TOTAL Leg FROM ALL SOURCES (DAY): 65.18 (NIGHT): 58.65

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:09:36

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b3north.te Time Period: Day/Night 16/8 hours

Description: Building #3 North Facade Floor 1

Road data, segment # 1: Howard Ave (day/night)

\_\_\_\_\_

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000
Percentage of Annual Growth : 2.50
Number of Years of Growth : 15.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Howard Ave (day/night)

-----

Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 60.00 / 60.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Dougal Pk Ea (day/night)

-----

Car traffic volume : 14497/1611 veh/TimePeriod \*
Medium truck volume : 305/34 veh/TimePeriod \*
Heavy truck volume : 458/51 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 2.50

Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 2: Dougal Pk Ea (day/night) -----Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface) Receiver source distance : 310.00 / 310.00 m Receiver height : 2.00 / 2.00 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle : 0.00 Road data, segment # 3: Dougal Pk So (day/night) \_\_\_\_\_ Car traffic volume : 5557/617 veh/TimePeriod \* Medium truck volume : 117/13 veh/TimePeriod \* Heavy truck volume : 175/19 veh/TimePeriod \* Posted speed limit : 60 km/h Road gradient : Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 4600 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 3: Dougal Pk So (day/night) Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods Wood depth : 0
No of house rows : 0 / 0
Surface : 2 (No woods.) 2 Surface (Reflective ground surface)

: 1 (Flat/gentle slope; no barrier)

Results segment # 1: Howard Ave (day)

Reference angle : 0.00

Topography

Receiver source distance : 320.00 / 320.00 m Receiver height : 2.00 / 2.00 m  $\,$ 

\_\_\_\_\_\_

Segment Leq: 59.68 dBA

Results segment # 2: Dougal Pk Ea (day)

Source height = 1.32 m

ROAD (0.00 + 55.27 + 0.00) = 55.27 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 68.42 0.00 -13.15 0.00 0.00 0.00 0.00 55.27

Segment Leq: 55.27 dBA

Results segment # 3: Dougal Pk So (day)

Source height = 1.32 m

ROAD (0.00 + 50.96 + 0.00) = 50.96 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 64.25 0.00 -13.29 0.00 0.00 0.00 0.00 50.96

Segment Leq: 50.96 dBA

Total Leq All Segments: 61.43 dBA

Results segment # 1: Howard Ave (night)

Source height = 1.32 m

Segment Leq : 53.14 dBA

Results segment # 2: Dougal Pk Ea (night)

Source height = 1.32 m

ROAD (0.00 + 48.74 + 0.00) = 48.74 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq - 90 90 0.00 61.89 0.00 -13.15 0.00 0.00 0.00 0.00 48.74

\_\_\_\_\_\_

Segment Leq: 48.74 dBA

Results segment # 3: Dougal Pk So (night)

Source height = 1.31 m

ROAD (0.00 + 44.37 + 0.00) = 44.37 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 57.66 0.00 -13.29 0.00 0.00 0.00 0.00 44.37

Segment Leq: 44.37 dBA

Total Leq All Segments: 54.89 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 61.43 (NIGHT): 54.89

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:10:23

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b3east.te Time Period: Day/Night 16/8 hours

Description: Building #3 East Facade Floor 1

Road data, segment # 1: North Talbot (day/night)

-----

Car traffic volume : 12781/1420 veh/TimePeriod \*
Medium truck volume : 269/30 veh/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 128.00 / 128.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Dougal Pk Ea (day/night)

-----

Car traffic volume : 14497/1611 veh/TimePeriod \*
Medium truck volume : 305/34 veh/TimePeriod \*
Heavy truck volume : 458/51 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 2.50

Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 2: Dougal Pk Ea (day/night) -----Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 (No woods No of house rows : 0 / 0 Surface : 2 (Reflect: (No woods.) (Reflective ground surface) Receiver source distance : 315.00 / 315.00 m Receiver height : 2.00 / 2.00 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle : 0.00 Road data, segment # 3: Dougal Pk So (day/night) -----Car traffic volume : 5557/617 veh/TimePeriod \* Medium truck volume : 117/13 veh/TimePeriod \* Heavy truck volume : 175/19 veh/TimePeriod \* Posted speed limit : 60 km/h Road gradient : Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 4600 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

#### Data for Segment # 3: Dougal Pk So (day/night)

Angle1 Angle2 : -90.00 deg Wood depth : 0 0.00 deg Wood depth : 0
No of house rows : 0 / 0
Surface : 2 (No woods.)

0 / 0

2 Surface (Reflective ground surface)

Receiver source distance : 325.00 / 325.00 m Receiver height : 2.00 / 2.00

: 1 (Flat/gentle slope; no barrier) Topography

Reference angle : 0.00

Results segment # 1: North Talbot (day)

Source height = 1.32 m

ROAD (0.00 + 53.97 + 0.00) = 53.97 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 66.29 0.00 - 9.31 - 3.01 0.00 0.00 0.00 53.97

Segment Leq: 53.97 dBA

Results segment # 2: Dougal Pk Ea (day)

Source height = 1.32 m

ROAD (0.00 + 52.19 + 0.00) = 52.19 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

Segment Leq: 52.19 dBA

Results segment # 3: Dougal Pk So (day)

-----

Source height = 1.32 m

ROAD (0.00 + 47.88 + 0.00) = 47.88 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

Segment Leq: 47.88 dBA

Total Leq All Segments: 56.78 dBA

Results segment # 1: North Talbot (night)

-----

Source height = 1.32 m

ROAD (0.00 + 47.45 + 0.00) = 47.45 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 59.77 0.00 - 9.31 - 3.01 0.00 0.00 0.00 47.45

-----

Segment Leq: 47.45 dBA

Results segment # 2: Dougal Pk Ea (night)

Source height = 1.32 m

ROAD (0.00 + 45.66 + 0.00) = 45.66 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

Segment Leq: 45.66 dBA

Results segment # 3: Dougal Pk So (night)

-----

Source height = 1.31 m

ROAD (0.00 + 41.29 + 0.00) = 41.29 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-----

Segment Leq: 41.29 dBA

Total Leq All Segments: 50.25 dBA

TOTAL Leg FROM ALL SOURCES (DAY): 56.78

(NIGHT): 50.25

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:09:58

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b3south.te Time Period: Day/Night 16/8 hours

Description: Building #3 South Facade Floor 1

Road data, segment # 1: North Talbot (day/night)

-----

Car traffic volume : 12781/1420 veh/TimePeriod \*
Medium truck volume : 269/30 veh/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg

Wood depth : 0 (No woods.)
No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 130.00 / 130.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Howard Ave (day/night)

-----

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000 Percentage of Annual Growth : 2.50 Number of Years of Growth : 15.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 2: Howard Ave (day/night)

-----

: 0.00 deg 90.00 deg : 0 (No woods Angle1 Angle2 Wood depth (No woods.)

No of house rows : 0 / 0

2 (Reflective ground surface) Surface

Receiver source distance : 34.00 / 34.00 m Receiver height : 2.00 / 2.00 m

: 1 (Flat/gentle slope; no barrier) Topography

: 0.00 Reference angle

Results segment # 1: North Talbot (day) \_\_\_\_\_

Source height = 1.32 m

ROAD (0.00 + 56.92 + 0.00) = 56.92 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_

- 90 90 0.00 66.29 0.00 - 9.38 0.00 0.00 0.00 0.00 56.92 \_\_\_\_\_\_

Segment Leq: 56.92 dBA

Results segment # 2: Howard Ave (day)

\_\_\_\_\_

Source height = 1.32 m

ROAD (0.00 + 62.14 + 0.00) = 62.14 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_\_ 0 90 0.00 68.71 0.00 - 3.55 - 3.01 0.00 0.00 0.00 62.14

\_\_\_\_\_\_

Segment Leq: 62.14 dBA

Total Leq All Segments: 63.28 dBA

Results segment # 1: North Talbot (night)

Source height = 1.32 m

Segment Leq: 50.39 dBA

Results segment # 2: Howard Ave (night)

Source height = 1.32 m

ROAD (0.00 + 55.60 + 0.00) = 55.60 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 62.17 0.00 - 3.55 - 3.01 0.00 0.00 0.00 55.60

Segment Leq: 55.60 dBA

Total Leq All Segments: 56.74 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 63.28 (NIGHT): 56.74

STAMSON 5.0 NORMAL REPORT Date: 07-09-2023 17:10:36

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: b3west.te Time Period: Day/Night 16/8 hours

Description: Building #3 West Facade Floor 1

Road data, segment # 1: North Talbot (day/night)

-----

Car traffic volume : 12781/1420 veh/TimePeriod \*
Medium truck volume : 269/30 veh/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 142.00 / 142.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Howard Ave (day/night)

-----

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000 Percentage of Annual Growth : 2.50

Number of Years of Growth : 15.00 Medium Truck % of Total Volume : 2.00 Heavy Truck % of Total Volume : 3.00 Day (16 hrs) % of Total Volume : 90.00

#### Data for Segment # 2: Howard Ave (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth (No woods.) : 0

No of house rows : 0 / 0

2 Surface (Reflective ground surface)

Receiver source distance : 39.00 / 39.00 m Receiver height : 2.00 / 2.00

: 1 (Flat/gentle slope; no barrier) Topography

Reference angle : 0.00

#### Road data, segment # 3: Dougal Pk Ea (day/night)

Car traffic volume : 14497/1611 veh/TimePeriod \* Medium truck volume: 305/34 veh/TimePeriod \* Heavy truck volume : 458/51 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

: 1 (Typical asphalt or concrete) Road pavement

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 2.50 Number of Years of Growth : 14.00 Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

#### Data for Segment # 3: Dougal Pk Ea (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth 0 (No woods.) Wood depth
No of house rows

0 / 0

Surface 2 (Reflective ground surface)

Receiver source distance : 315.00 / 315.00 m Receiver height : 2.00 / 2.00 m

1 (Flat/gentle slope; no barrier) Topography

Reference angle : 0.00

Road data, segment # 4: Dougal Pk So (day/night)

-----

Car traffic volume : 5557/617 veh/TimePeriod \*

Medium truck volume : 117/13 veh/TimePeriod \* Heavy truck volume : 175/19 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4600
Percentage of Annual Growth : 2.50
Number of Years of Growth : 14.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 4: Dougal Pk So (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.)

Wood depth : 0
No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 325.00 / 325.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: North Talbot (day)

Source height = 1.32 m

ROAD (0.00 + 53.52 + 0.00) = 53.52 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 66.29 0.00 - 9.76 - 3.01 0.00 0.00 0.00 53.52

Segment Leq: 53.52 dBA

Results segment # 2: Howard Ave (day)

Source height = 1.32 m

.-----

Segment Leq: 64.56 dBA

Results segment # 3: Dougal Pk Ea (day)

Source height = 1.32 m

ROAD (0.00 + 52.19 + 0.00) = 52.19 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 68.42 0.00 -13.22 - 3.01 0.00 0.00 0.00 52.19

Segment Leq: 52.19 dBA

Results segment # 4: Dougal Pk So (day)

\_\_\_\_\_

Source height = 1.32 m

ROAD (0.00 + 47.88 + 0.00) = 47.88 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 64.25 0.00 -13.36 - 3.01 0.00 0.00 0.00 47.88

-----

Segment Leq: 47.88 dBA

Total Leq All Segments: 65.20 dBA

Results segment # 1: North Talbot (night)

-----

Source height = 1.32 m

ROAD (0.00 + 47.00 + 0.00) = 47.00 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 59.77 0.00 - 9.76 - 3.01 0.00 0.00 0.00 47.00

Segment Leq: 47.00 dBA

Results segment # 2: Howard Ave (night)

Source height = 1.32 m

ROAD (0.00 + 58.02 + 0.00) = 58.02 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ - 90 90 0.00 62.17 0.00 - 4.15 0.00 0.00 0.00 0.00 58.02

Segment Leq: 58.02 dBA

Results segment # 3: Dougal Pk Ea (night) \_\_\_\_\_

Source height = 1.32 m

ROAD (0.00 + 45.66 + 0.00) = 45.66 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ 90 0.00 61.89 0.00 -13.22 - 3.01 0.00 0.00 0.00 45.66 \_\_\_\_\_\_

Segment Leq: 45.66 dBA

Results segment # 4: Dougal Pk So (night) \_\_\_\_\_

Source height = 1.31 m

ROAD (0.00 + 41.29 + 0.00) = 41.29 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq \_\_\_\_\_\_ 90 0.00 57.66 0.00 -13.36 - 3.01 0.00 0.00 0.00 41.29 \_\_\_\_\_\_

Segment Leq: 41.29 dBA

Total Leq All Segments: 58.66 dBA

TOTAL Leg FROM ALL SOURCES (DAY): 65.20

(NIGHT): 58.66

STAMSON 5.0 NORMAL REPORT Date: 08-09-2023 12:18:19

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: ola.te Time Period: Day/Night 16/8 hours

Description: Outdoor Living Area

Road data, segment # 1: North Talbot (day/night)

Car traffic volume : 12781/1420 veh/TimePeriod \*
Medium truck volume : 269/30 veh/TimePeriod \*
Heavy truck volume : 404/45 veh/TimePeriod \*

Posted speed limit : 50 km/h
Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8900
Percentage of Annual Growth : 2.50
Number of Years of Growth : 21.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: North Talbot (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 120.00 / 120.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: Howard Ave (day/night)

-----

Car traffic volume : 22289/2477 veh/TimePeriod \*
Medium truck volume : 469/52 veh/TimePeriod \*
Heavy truck volume : 704/78 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 0 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 18000 Percentage of Annual Growth : 2.50 Number of Years of Growth : 15.00
Medium Truck % of Total Volume : 2.00
Heavy Truck % of Total Volume : 3.00
Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 2: Howard Ave (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 2 (Reflective ground surface)

Receiver source distance : 42.00 / 42.00 m Receiver height : 2.00 / 2.00 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: North Talbot (day)

-----

Source height = 1.32 m

ROAD (0.00 + 57.26 + 0.00) = 57.26 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 66.29 0.00 - 9.03 0.00 0.00 0.00 0.00 57.26

Segment Leq: 57.26 dBA

Results segment # 2: Howard Ave (day)

-----

Source height = 1.32 m

ROAD (0.00 + 64.24 + 0.00) = 64.24 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 68.71 0.00 - 4.47 0.00 0.00 0.00 0.00 64.24

-----

Segment Leq: 64.24 dBA

Total Leq All Segments: 65.03 dBA

Results segment # 1: North Talbot (night)

-----

Source height = 1.32 m

ROAD (0.00 + 50.74 + 0.00) = 50.74 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 59.77 0.00 - 9.03 0.00 0.00 0.00 0.00 50.74

Segment Leq: 50.74 dBA

Results segment # 2: Howard Ave (night)

Source height = 1.32 m

ROAD (0.00 + 57.70 + 0.00) = 57.70 dBA

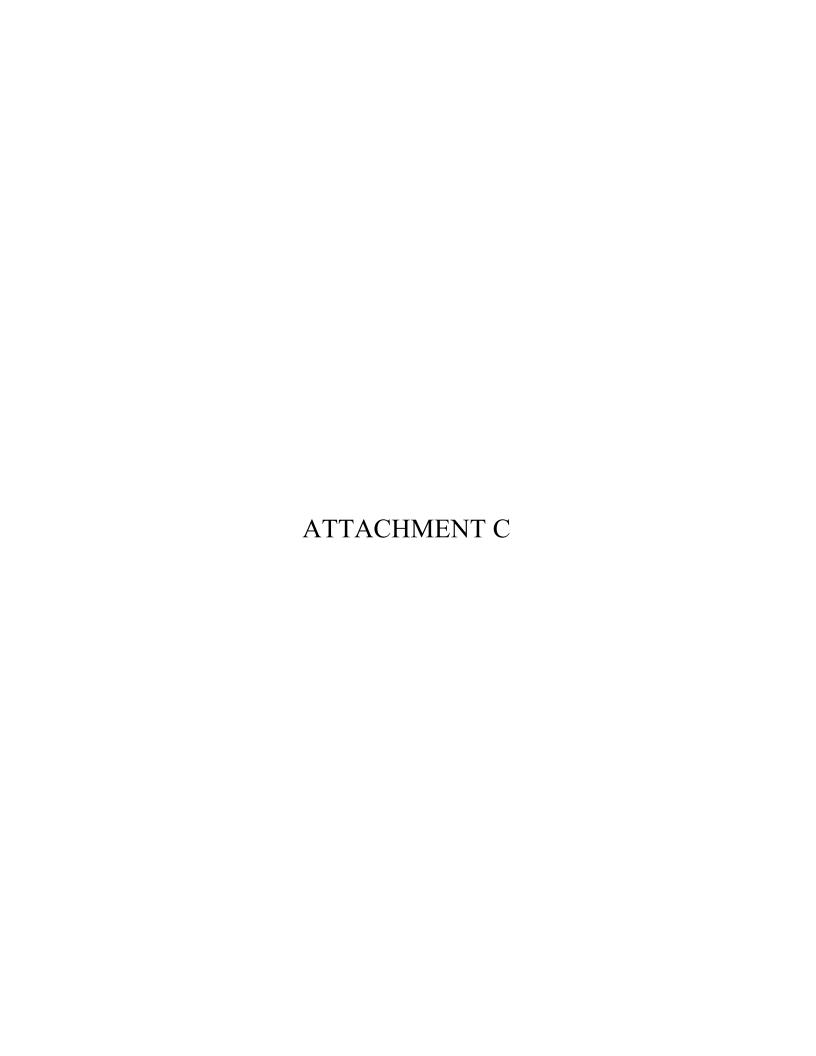
Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

- 90 90 0.00 62.17 0.00 - 4.47 0.00 0.00 0.00 0.00 57.70

Segment Leq: 57.70 dBA

Total Leq All Segments: 58.50 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 65.03 (NIGHT): 58.50





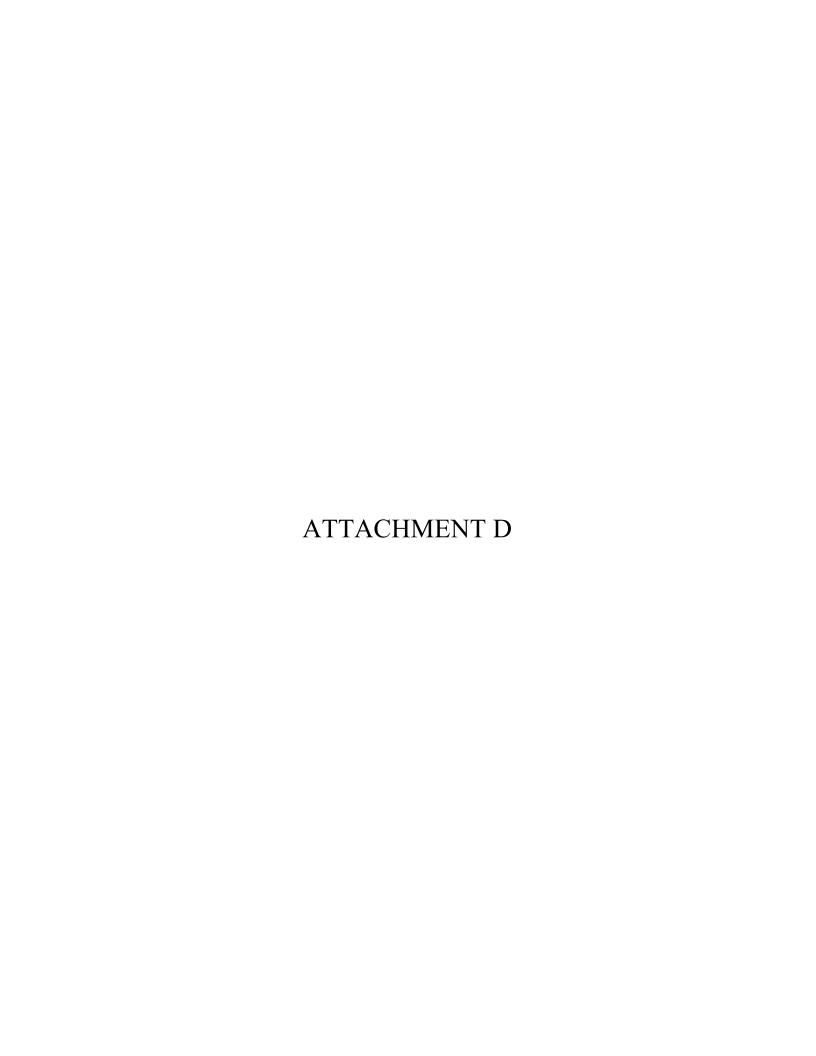


Table D1
Stationary Noise Impact Source Data
4280 Howard Place, Windsor, Ontario

		Total	Data Source	Height			
		SWL	or	Absolute	<b>Above Roof</b>		
Noise Source Description	Cadna ID	(dBA)	Representative Data	(m)	(m)	х	у
Small HVAC	Small_HVAC	81.9	Small_HVAC	6.5	1.5	17335337.8	4679056
Small HVAC	Small_HVAC	81.9	Small_HVAC	6.5	1.5	17335336.4	4679051
Small HVAC	Small_HVAC	81.9	Small_HVAC	6.5	1.5	17335338.3	4679047
Small HVAC	Small_HVAC	81.9	Small_HVAC	9.5	1.5	17335328.9	4679019
Small HVAC	Small_HVAC	81.9	Small_HVAC	9.5	1.5	17335332.7	4679015
Small HVAC	Small_HVAC	81.9	Small_HVAC	9.5	1.5	17335337.5	4679013





October 3, 2023

Corporation of the City of Windsor Engineering Department – Development Division 350 City Hall Square West, Room 210 Windsor, Ontario, N9A 6S1

ATT: MR. ROBERT PERISSINOTTI, DEVELOPMENT ENGINEER

RE: SANITARY SEWER STUDY FOR THE PROPOSED RESIDENTIAL DEVELOPMENT AT

**0 HOWARD AVENUE, WINDSOR, ONTARIO** 

Dear Mr. Perissinotti.

We were retained by Architectural Design Associates Inc. to conduct a sanitary sewer study for the proposed residential development at 0 Howard Avenue which is required at this time for a zoning by-law amendment.

The property is currently an undeveloped open grass area and is a zoned commercial district. Proposed are three multi-unit buildings each with 6 units for a total of 18 units.

The existing municipal sanitary sewer system has been assessed to determine if there is capacity available to accept the increased sewage flow from the proposed medium density residential development. The sewer analyzed is the 250 mm diameter PVC sanitary sewer along Howard Place. This sanitary sewer transitions to a 900 mm diameter sanitary trunk sewer at the Howard Avenue & North Talbot intersection.

The existing 250 mm diameter sanitary sewer along Howard Place has a gradient of 0.41% and a total capacity of 38 L/s. The sewer currently provides drainage solely for the fourteen (14) single family dwellings along Howard Place.

The peak sewage flow rate from these existing dwellings to the municipal sewer is approximately 1.4 L/s based on a population density of 3.5 persons per household. The proposed medium density residential development will have 18 units for a total population of 38 persons based on a 2.1 person per unit population density. This corresponds to a peak domestic sewage flow rate of 0.8 L/s. Therefore, the total peak sewage flow rate in the proposed condition would be approximately 2.2 L/s.

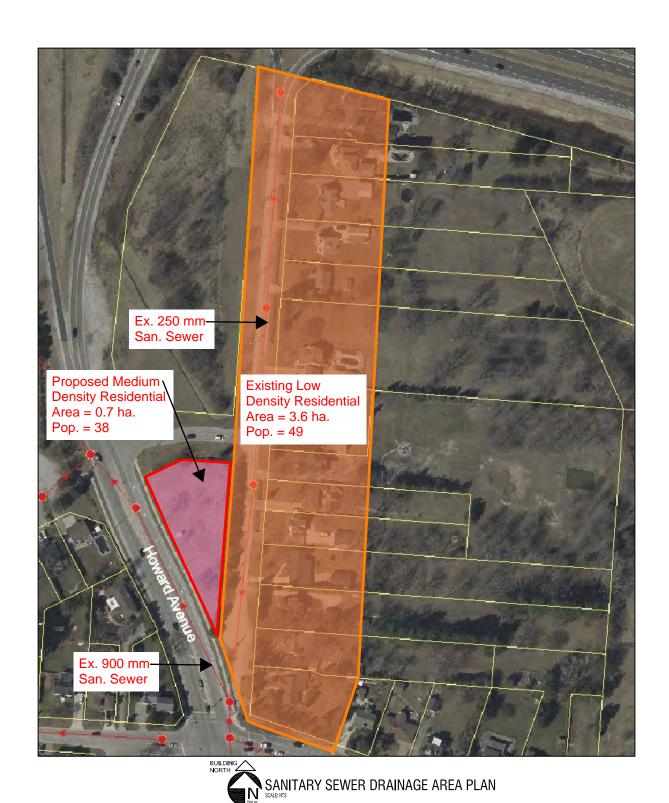
As indicated, the existing municipal sanitary sewer has a capacity of 38 L/s and will therefore only have 6% of its capacity utilized. Please refer to the sanitary sewer capacity assessment enclosed. The assessed municipal sanitary sewer has substantial capacity available to support the proposed development.

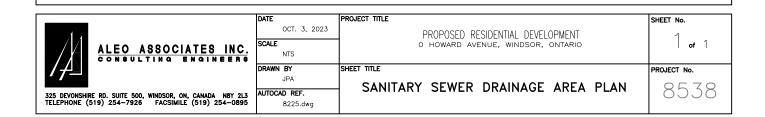
If you have any questions or concerns, please contact me.

Yours Very Truly

John-Paul Aleo, P.Eng. ALEO ASSOCIATES INC.







#### **ALEO ASSOCIATES INC.**

**Consulting Engineers** 

Prepared By: J.P.A.

Project Name: Howard Residential Development

Project Address: 0 Howard Avenue

Project No.: 8538

Date: 2023.09.26

# SANITARY SEWER CAPACITY ASSESSMENT 250 mm DIAMETER SANITARY SEWER FROM MH 7S3173 TO MH 7S3174 ASSESSMENT OF PROPOSED CONDITION

LOCATION			POPULATION		SEWAGE FLOW			SEWER DESIGN							
Area No.	DEVELOPMENT TYPE	AREA (HEC.)	# OF UNITS	PER UNIT	POP.	PEAKING FACT.	INFIL. I/sec	SEW. I/sec	TOTAL l/sec	SIZE (mm)	n	SLOPE (%)	CAP. I/sec	VEL. m/s	CAPACITY UTILIZED (%)
1	SINGLE-FAMILY DWELLINGS (LOW DENSITY RESIDENTIAL)	3.6	14	3.5	49	4.3	0.6	0.9	1.4	-	-	-	,	-	-
2	PROPOSED 6 PLEX DEVELOPMENT (MEDIUM DENSITY RESIDENTIAL)	0.7	18	2.1	38	4.3	0.1	0.7	0.8	•	-	-	1	•	-
	TOTAL	112.0		-	87	-	0.7	1.6	2.2	250	0.013	0.41	38	0.78	5.9

Design Criteria:

2) Infiltration =

1) Residential Sewage Flow Rate =

0.0042 sec/cap 0.1560 l/s/ha

3) Peak Wastewater Flow Factor, M =

1+14/(4+P^0.5)

4) Manning's Coefficient =

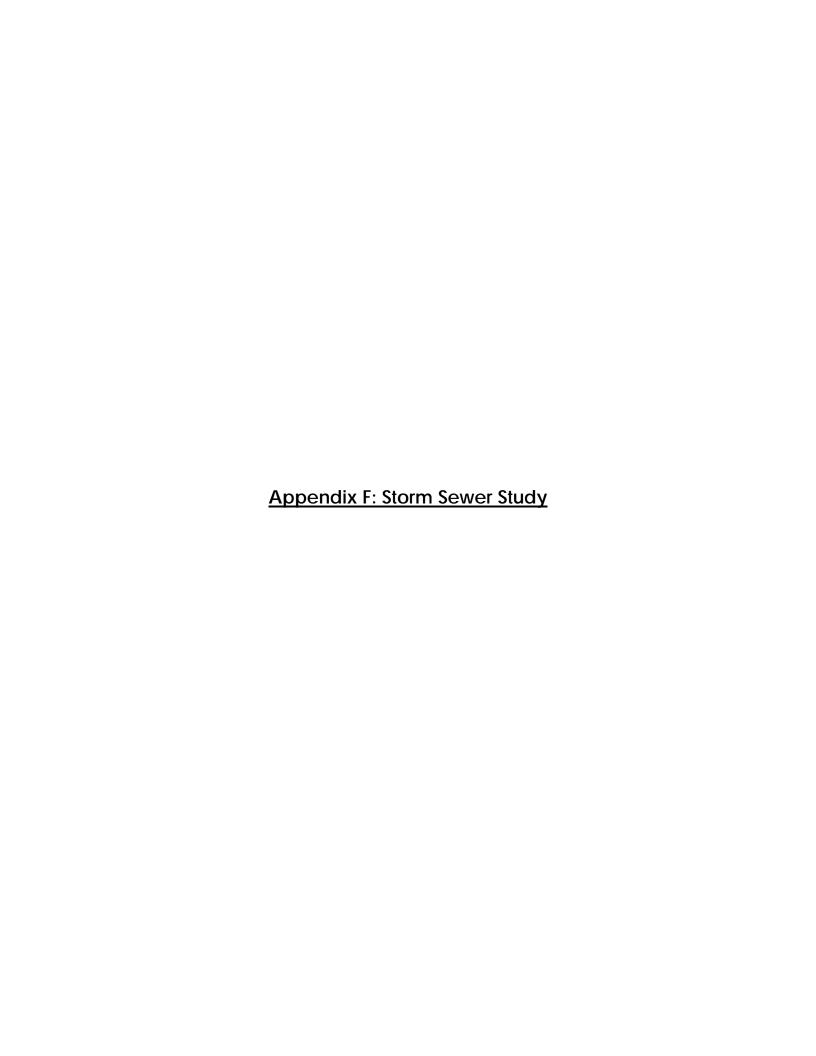
0.013

5) Minimum Velocity =

0.76 m/s

6) Maximum Velocity =

3.0 m/s





October 3, 2023

Corporation of the City of Windsor Engineering Department – Development Division 350 City Hall Square West, Room 210 Windsor, Ontario, N9A 6S1

ATT: MR. ROBERT PERISSINOTTI, DEVELOPMENT ENGINEER

RE: STORM SEWER STUDY FOR THE PROPOSED RESIDENTIAL DEVELOPMENT AT

**0 HOWARD AVENUE. WINDSOR, ONTARIO** 

Dear Mr. Perissinotti,

We have been retained by Architectural Design Associates Inc. to conduct a storm sewer study for the proposed residential development at 0 Howard Avenue which is required at this time for a zoning by-law amendment.

The property is bounded by Howard Avenue to the West, Howard Place to the East, Tuson Way to the North, and North Talbot Road to the South. See site location drawing enclosed.

The property has a total area of 29,664 ft² (0.681 acres) and is currently an undeveloped open grass area. The property is generally flat with the land sloping from South to North. The land currently drains stormwater runoff by overland flow to an existing municipal ditch inlet catch basin located North-East of the site. See topographic survey plan enclosed showing the drainage pattern of the land.

The pre-development release rate to be used for the proposed development shall be based on the current overland flow rate from the undeveloped open grass area to the municipal drainage system. The pre-development release rate was determined to be 7 L/s based on a hydrologic analysis using the 1:2 year 4-hour Chicago design storm distribution. See determination of the pre-development release rate enclosed.

The proposed development consists of three, multi-unit residential buildings with surrounding parking lot and landscape areas. An 80% impervious percentage will be used for the developed site. A flow restrictor will be installed at the outlet to restrict the post development flows to the pre-development release of 7 L/s. The runoff rate of the existing pre-developed condition is being maintained as part of the proposed development and therefore, there will not be any effect on the receiving storm sewer system or surrounding properties.

A storm detention scheme will be carried out during the detailed design phase and will be completed to conform to the Windsor-Essex Region Stormwater Management Standards. Storage will be provided through surface storage on the parking lot surface and in an underground chamber system.

Stormwater quality control will be accomplished through the underground chamber system which will treat stormwater captured from the site through a settling and filtration process before it is released to the municipal sewer system. The level of treatment will be normal (70% TSS removal).

If you have any questions or concerns, please contact me.

Yours Very Truly,

John-Paul Aleo, P.Eng.

**ALEO ASSOCIATES INC.** 

Oct. 03, 2023





OCT. 3, 2023  SCALE  NTS	PROPOSED RESIDENTIAL DEVELOPMENT o howard avenue, windsor, ontario	SHEET No.
JPA AUTOCAD REF. 8225.dwg	SHEET TITLE SITE LOCATION	PROJECT No. 8538

#### **Pre-Development Release Rate:**

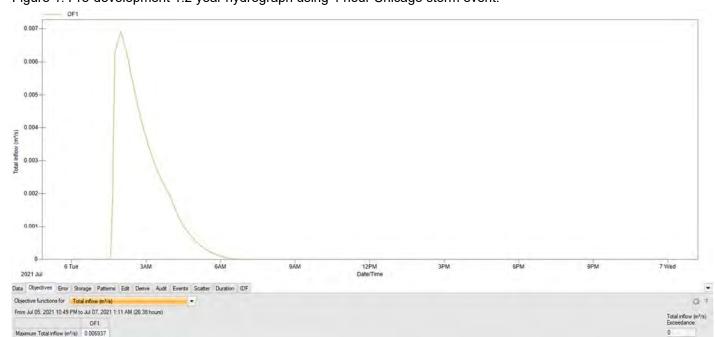
A PCSWMM model was prepared to simulate the existing drainage condition of the site and to determine the predevelopment release rate for the property. The site was modelled as a single catchment area and using the Green-Ampt Infiltration method. The land is currently an open grass area with numerous trees. The native soil consists of Berrien Sand which is classified as hydrologic soil group 'C'. The pre-development release rate model ran the 1:2-year 4-hour Chicago storm event with a 15-minute time interval and a total rainfall depth of 37.7 mm. Provided in the table below are the sub-catchment parameters used.

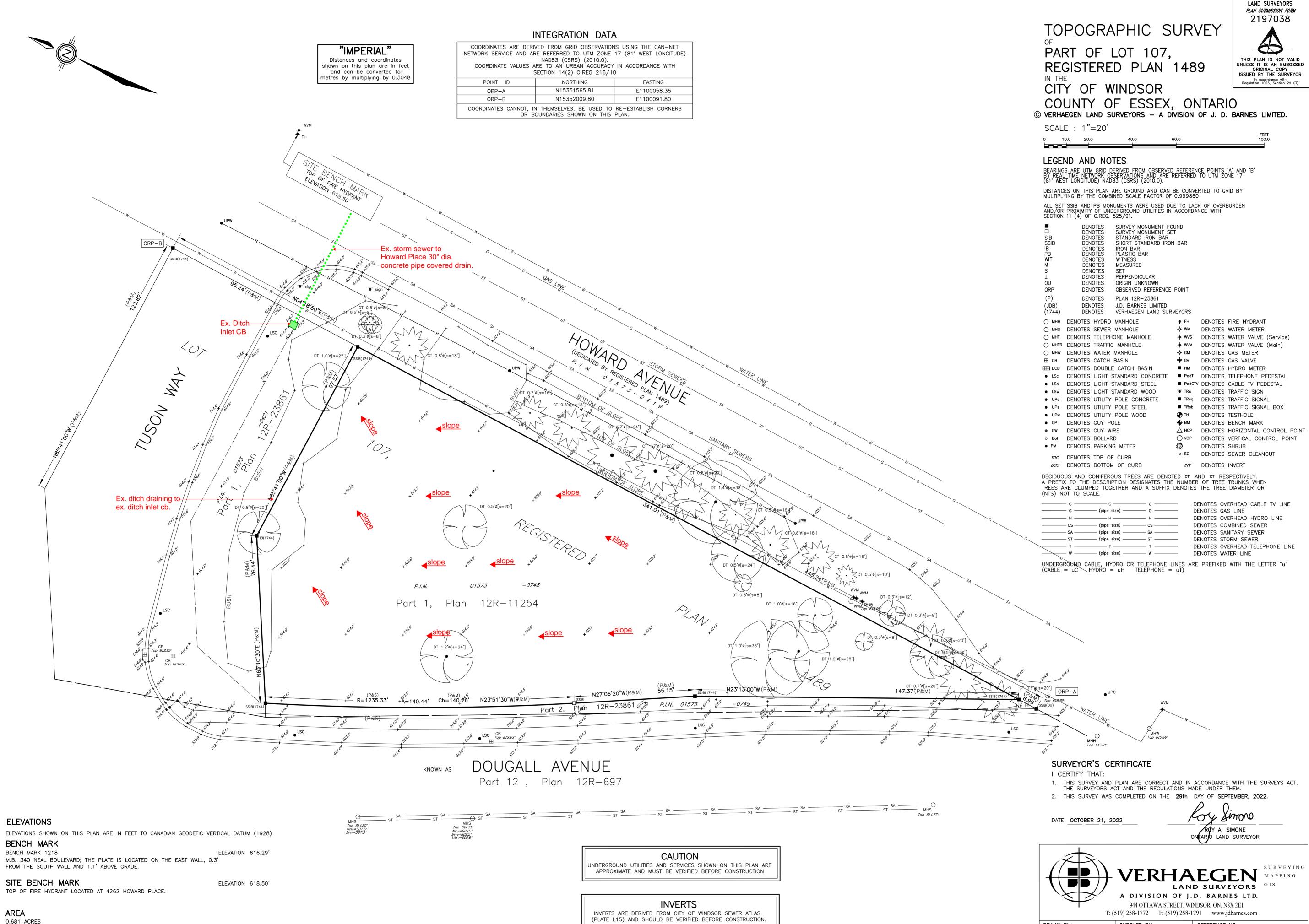
Table 1: Sub-catchment Parameters for the Pre-Development Release Rate Model

Attri	bute	Value		
Area	(Ha.)	0.28		
Flow Le	ngth (m)	103		
Flow W	idth (m)	27		
Percent of Impe	rvious Area (%)	0		
Slope	∈ (%)	1.0		
Manning's n for	Impervious Area	0.013		
Manning's n F	Pervious Area	0.24 (grass dense)		
Depression Storag	e Impervious (mm)	2.5		
Depression Stora	ge Pervious (mm)	10.0 (open field)		
Green-Ampt Infiltration	Suction Head (mm)	180		
Soil Type: Berrien Sand	Conductivity (mm/hr)	0.50		
Hydrologic Group 'C'	Initial Deficit, normal	0.10		

Based on the existing condition, the pre-development release rate for the proposed drainage area was determined to be 7 L/s. Refer to Figure 1.

Figure 1: Pre-development 1:2 year hydrograph using 4 hour Chicago storm event.





DRAWN BY:

A.J.M.

FILE: 22-47-404-00.dwg

CHECKED BY:

E-1489-10

R.A.S.

REFERENCE NO .:

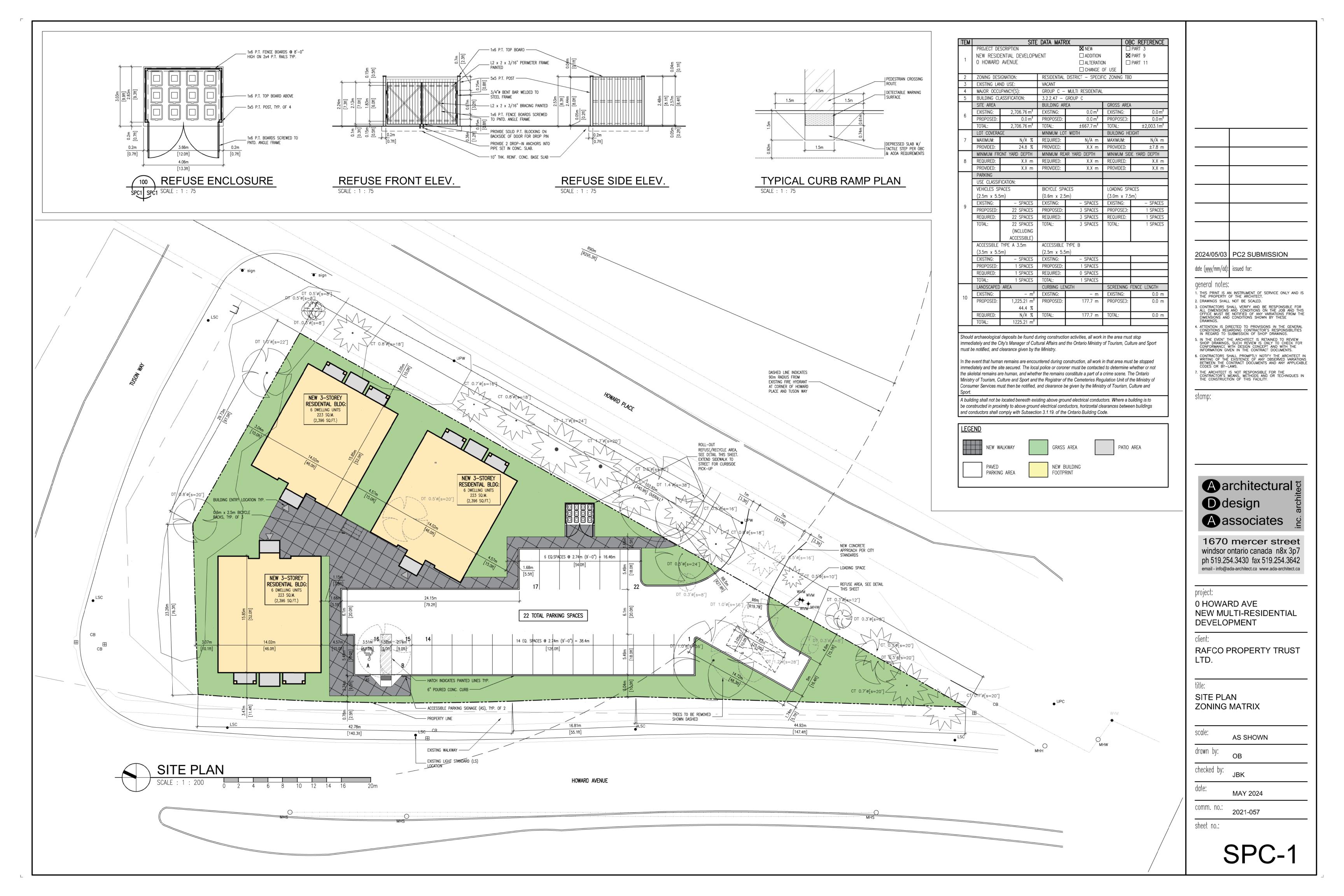
22-47-404-00

CAD Date: October 21, 2022 11:25 AM

CAD File: 22-47-404-00.dwg

ASSOCIATION OF ONTARIO









November 12, 1992

Imperial Oil Ltd. 90 Wynford Drive North York, Ontario M3C 1K5

Attention: Mr. John Marshall

RE: SUBSURFACE INVESTIGATION

Former Texaco Service Station

4280 Howard Avenue Windsor, Ontario

Dear Sir:

The following report documents work completed by Central Projects Group Inc. (CPG) on September 29 and September 30, 1992 at the above location. The purpose of the work was to investigate and address possible remaining environmental concerns associated with the past use of the property as a Texaco service station. This work was requested by Imperial Oil Ltd. (IOL) with respect to the divestment and potential sale of the property.

Our investigations and remedial work were conducted as a follow-up to investigations conducted by Golder Associates (GA) in April, 1989 (refer to GA report dated, April 5, 1989).

The following report summarizes our findings as of September 30, 1992.

CPG's summary regarding the environmental condition of the property prior to our investigative work, based on our review of the GA report, and information obtained through discussions with Mr. John Marshall of IOL, are as follows:

The soils underlying the site consist of fill overlying a native silty clay till. The
fill consists of similar silty clay till, mixed with topsoil and granular material,
ranging in thickness between 0.6 and 2.9 m.

Groundwater was observed in boreholes, ranging between 0.63 and 0.86 m below grade following a gentle southerly gradient. Hydraulic conductivity of the soil was determined to be low (GA 1989).

- Hydrocarbon impact of soils identified in the 1989 GA report was limited to a
  maximum of 150 parts per million (ppm) based on laboratory analysis for total
  oil and grease in representative "worst case" samples (GA 1989).
- Hydrocarbon impact in groundwater samples analyzed for total oil and grease was limited to a maximum of 3 milligrams per litre (GA 1989).
- At the time of the GA study, all structures and equipment had been removed including six (6) UST's utilized for product storage.
- Investigative work completed by GA did not reveal the presence of significant petroleum hydrocarbon impact. Oil & grease concentrations in both soil and groundwater samples were within Ontario MOE clean-up criteria (GA 1989).

- Future intended land use is unknown.
- The subject site's sensitivity was determined using the sensitivity matrix outlined in the Province of Alberta's "Subsurface Remediation Guidelines for Underground Storage Tanks February 1991", commonly referred to as the "MUST" Guidelines. Based on the analysis, the site would be classified as "moderately" sensitive and hence, MUST Level II would apply.

#### September 29, 1992

On September 29, 1992, CPG personnel conducted a site reconnaissance and testpitting program using a rubber-tire backhoe.

The site reconnaissance included the monitoring of the accessible groundwater monitors installed at the site by GA. This monitoring included measuring of the Total Organic Vapour (TOV) concentrations with a portable Gastechtor Model 1238.

The TOV concentrations were measured with a Gastechtor Model 1238, calibrated with hexane. The Gastechtor is capable of detecting TOV concentrations from 0 to 12,000 ppm where 120 ppm is equivalent to 1 %LEL.

The measured TOV concentrations were predominantly low (<175 ppm) in the existing BH2, BH5, and BH6 (refer to Figure 1 for locations of monitors and TOV readings). The TOV concentration in BH3 measured 100% LEL, presumed to be chiefly methane based on a strong organic, non-fuel related odour. BH1 and BH4 could not be located. Phase separated liquid hydrocarbon was not encountered in any of the monitoring wells on this date.

A total of six (6) testpits were excavated at the locations shown in Figure 1. The testpits generally confirmed the findings of the earlier investigation. Other findings include:

- Some product piping of the former fuelling system was still present in the subsurface and was removed where encountered.
- Testpit 1 (TP1) was dug to a depth of 3.4 m below grade in the vicinity of the former tank farm (Figure 1). Grey/black staining, as well as asphalt debris, was observed in the clayey backfill. A slight hydrocarbon odour was present throughout the material to the bottom of the testpit until native, hard brown silty clay was reached, which was free of hydrocarbon odour and staining (refer to Table 1 for TOV readings). Groundwater was encountered at 3.0 m below grade.
- TP2 was started near TP1 and advanced southward in order to intersect the most southerly limit of the tank farm. Observations were similar to TP1 until the native bank was reached where the hard, brown silty clay was free of staining and hydrocarbon odour. Perched groundwater was encountered at 1.8 m below grade, trapped in concrete rubble.
- TP3 was dug to 2.5 m below grade; minor grey staining, no hydrocarbon odour.
   Groundwater was not encountered.
- TP4 was advanced to 1.9 m below grade; product piping unearthed; minor grey staining, no hydrocarbon odour.
- TP5 was excavated to just below the surface in an area of stained grass. Removal
  of the grass revealed brown granular material free of staining and hydrocarbon
  odour.

 TP6 was dug in the area of the former hoist within the former building. No evidence of hydrocarbons was present in the granular backfill.

The accumulated water in the open excavations did not exhibit the presence of phase separated-liquid hydrocarbons during our assessment activity on September 29, 1992.

One soil sample (S1-A) was taken from TP1, representing "worst case" conditions encountered at the site. One soil sample (S3-A) was taken from each of TP2, TP3 and TP4, and was combined as an aggregate sample, representing general site conditions. One water sample (S2-A) was taken from BH3 to determine potential impact of groundwater, based on elevated TOV readings (refer to Figure 1 for sample locations).

Soil samples were submitted for analysis of total petroleum hydrocarbons (TPH) concentrations, as well as, benzene, toluene, ethylbenzene and xylene (BTEX) concentrations. Water sample S2-A was analyzed for BTEX concentrations (refer to Table 2 for sample results data as compared with Alberta MUST Clean-up Criteria).

The results of these laboratory analyses indicate that the tested soils and groundwater meet the Alberta MUST Clean-up Criteria for sites of moderate sensitivity (Level II).

#### DISCUSSION OF RESULTS

In summary, CPG's investigative activities at the former Texaco service station located at 4280 Howard Avenue in Windsor, Ontario revealed that significant hydrocarbon impact was not present in the investigated areas.

Marginally impacted soils were encountered in the fill material near TP1 and TP2. The impacted soil was in the form of "faint" hydrocarbon odours and some grey/black staining in the backfill material. The less permeable, native till was noted to be free of hydrocarbons.

Laboratory analyses of the soil samples extracted from soils remaining at the site further indicate that:

- The tested soils meets the Ontario Ministry of the Environment Decommissioning guidelines for the tested parameters (GA 1989).
- BTEX and TPH concentrations in the tested soils meets the Alberta MUST criteria for sites of moderate sensitivity (Level II).
- BTEX was not detected in the groundwater sample extracted from BH3.

The information presented in this report was obtained while conducting investigative activity at the former Texaco service station located at 4280 Howard Avenue in the City of Windsor, Ontario, authorized by Imperial Oil Ltd.

This report is believed to provide a reasonable assessment of the conditions at the site within the excavated areas only, as of September 30, 1992 and draws conclusions based on these findings. Subsurface conditions between and beyond the excavated areas may differ and become apparent during future subsurface work.

We trust that the foregoing information is what you require at the present time. However, should you have any further questions, please do not hesitate to contact the undersigned.

Yours truly,

CENTRAL PROJECTS GROUP INC.

Per. Robert J. Kollaard

- Figure 1 - Site Plan

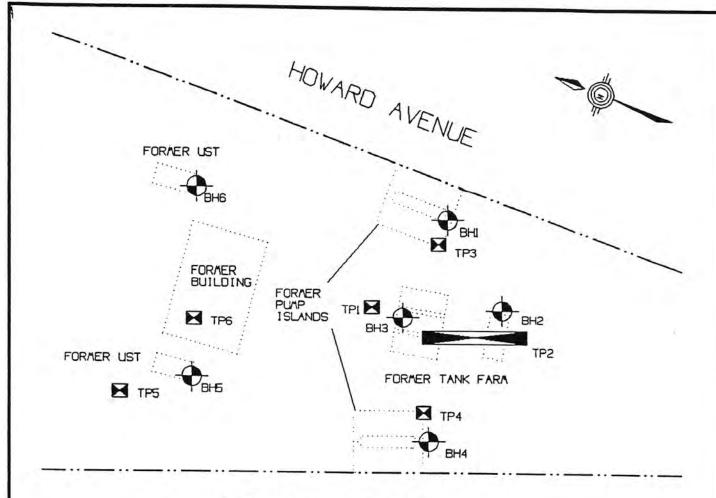
- Tables

- Appendix - Laboratory Analytical Results

Per. Harry H. Kim, P.Eng.

rd'esso31\rep.701

Attachments:



### DOUGALL AVENUE

NOTE: DRAVING NOT TO SCALE

TOV READINGS

SAMPLE LOCATIONS

BHI BH2 BH3 NOT FOUND

110 ppm 1007. LEL NOT FOUND 175 ppm 125 ppm

SI-A \$2-A \$3-A

VORST CASE: TPI VATER; BH3 AGGREGATE: TP2, TP3, TP4

## FORMER TEXACO SERVICE STATION

4280 HOWARD AVENUE WINDSOR, ONTARIO

SITE PLAN

JOB NO .:

DATE:

0701

10/04/92

DRAVING NO .:

FIGURE 1

# **TABLES**

**TABLE 1: Testpit Information** 

Test Location	Maximum TOV Concentration! (m below grade)	Maximum Depth (m below grade)	
TP1	5% LEL at 3.0	3.4	
TP2	120 at 1.8	1.8	
TP3	ND <sup>2</sup>	2.4	
TP4	ND	1.8	
TP5	ND	0.1	
TP6	ND	1.2	

<sup>1.</sup> All values in parts per million unless noted as % (%LEL)

TABLE 2: Testpit Soil Samples - Summary of Alberta MUST Related Laboratory Analyses

BOREHOLE NO.	DEPTH (m)	TPH (ppm)	BENZENE (ppm)	TOLUENE (ppm)	ETHYL- BENZENE (ppm)	XYLENE (ppm)	PHENOLS (ppm)	LEAD (ppm)
CRITERIA:								
MUST L	evel II	400	0.5	10.0	5.0	5.0	1.0	200
RESULTS:								
Sample S1-A	3.0	180	0.003	0.006	0.10	0.357	0.06	31.0
Sample S3-A	1.0	ND	ND	ND	ND	ND	NA	NA

<sup>1.</sup> All values in ppm

TABLE 3: Borehole Water Samples - Summary of Alberta MUST-Related Laboratory Analyses

BOREHOLE NO.	TPH (ppm)	BENZENE (ppm)	TOLUENE (ppm)	ETHYL- BENZENE (ppm)	XYLENE (ppm)	PHENOLS (ppm)	LEAD (ppm)
CRITERIA:							
MUST Level II	50	0.065	0.300	0.700	5	0.100	0.050
RESULTS!							
Sample S2-A	NA	ND	ND	ND	ND	NA	NA

<sup>1.</sup> All values in ppm

<sup>2.</sup> ND denotes not detected

<sup>2.</sup> ND - Not Detected, NA - Not Analyzed

<sup>2.</sup> ND - Not Detected, NA - Not Analyzed

# APPENDIX Laboratory Analytical Results

#### CLIENT INFORMATION

#### LABORATORY INFORMATION

Attention:

Robert Kollaard

Client Name:

Central Projects Group Inc.,

Project:

0701

Project Desc:

Howard/Dougal, Windsor

Address:

250 Shields Court.

Markham, Ontario

L3R 9W7

Fax Number:

416-470-0958

Phone Number: 416-470-6570

Contact:

Project:

Submission No.: 2J0088

Date Received: 92/10/05

Fax Number:

416-332-9169

Gerry Bengert

AN920840

Phone Number: 416-332-8788

NOTES:

All results are blank corrected except for Hi-Res MS data

'-' = Not Analysed

'<' = Less Than Method Detection Limit

Solids results are based on dry weight except for Volatile Organics, TPH and Biota analyses Organic analyses are not corrected for surrogate recoveries except for Isotope Dilution methods

Methods used by Zenon are based upon those found in 'Standard Methods for the Examination of Water and Wastewater'. Sixteenth Edition. published by the American Public Health Association, 1015 Fifteenth Street, NW, Washington, DC 20005. Other methods are based on the principles of MISA or EPA methodologies.

#### COMMENTS:

Certified by: A.A. Bengar 8

. #			3 2 - 0 - 0		
			Method	S1-A	S3-A Aggregate
	Client IL		Blank Soil	Worst Case	Conf.
	Zenon IL		028445 92	028446 92	028447 92
	Date Sample	t:	92/10/01	92/10/01	92/10/01
Component	MDL	Units			
Phenolics	0.01	mg/kg	<	0.06	E
Lead	10	mg/kg	<	31	-
ТРН	5	mg/kg	<	180	<
Surrogate Recoveries		%			
5-a-Androstane			85	113	118
Moisture	0.1	(%)		14	12
Benzene	0.001	mg/kg	<	0.003	<
Toluene	0.002		0.002	0.006	<
Ethylbenzene	0.002		<	0.10	<
m.p-Xylene	0.002		<	0.31	0.004
o-Xylene	0.002	*	<	0.047	0.003
Surrogate Recoveries		070			
d4-1,2-dichloroethane			108	85	108
d8-Toluene			101	74	93
Bromofluorobenzene			102	101	94

			Method	S2-A
	Client ID	:	Blank Water	Water BH3
	Zenon ID	:	028448 92	028449 92
	Date Sampled	:	92/10/01	92/10/01
Component	MDL	Units	107.000	4.5,4.
Benzene	0.2	ug/L	<.	<
Toluene	0.4	н	<	<
Ethyl Benzene	0.4	H.	<	<
m.p-Xylenes	0.5	6	<	<
o-Xylene	0.4	· • ·	<	<
Surrogate Recoveries		%		
d4-12-Dichloroethane			101	99
d8-Toluene			106	107
Bromofluorobenzene			102	101
			1.377	